



ELECTRIC POWER
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NDE of Reactor Materials

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Outline

- What's NDE?
- NDE for stainless steel and nickel-alloy components
 - Piping
 - Dissimilar metal welds
 - Cast stainless steel
 - Reactor pressure vessel head penetrations
- NDE for reactor pressure vessels
 - Vessel overview
 - Nozzles
 - Underclad cracking
 - Qualification
 - Example of plant-specific vessel NDE issue
- Summary

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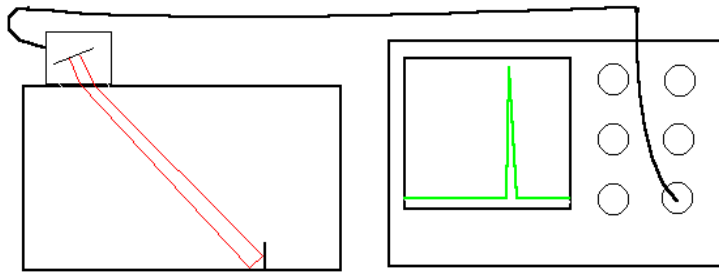
What's "NDE"?

- Nondestructive Evaluation
 - Inspecting components to see whether they're degraded, without damaging them
 - Cracking
 - Corrosion
 - Fabrication defects
 - Methods
 - Ultrasound
 - X-ray
 - Eddy current
 - Dye penetrant
- Examine the entire volume**
- Examine the surface**

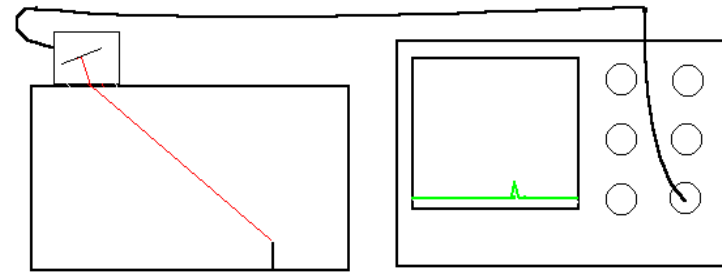
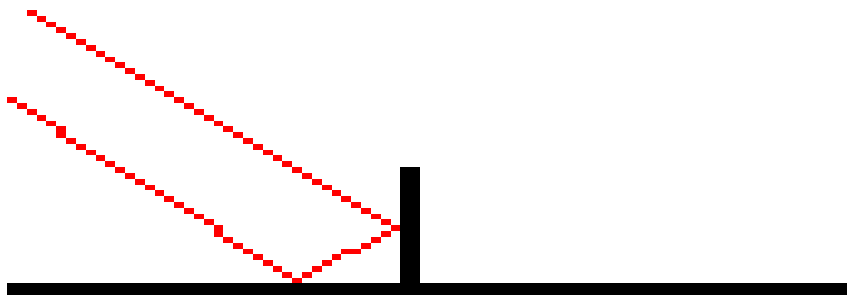
Ultrasonic examination (UT)

- Principle
 - Interaction of high frequency sound waves with the material (similar to sonar and medical ultrasound)
 - Reveals internal as well as surface breaking features
 - Most widely used inservice inspection method
 - Adaptable to many configurations & materials
 - Provides quantitative flaw location & sizing

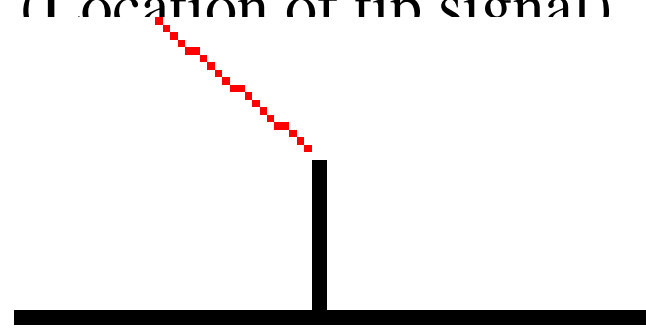
Basic pulse-echo UT



Detection
("corner echo")



Sizing
(Location of first signal)



Phased Array UT

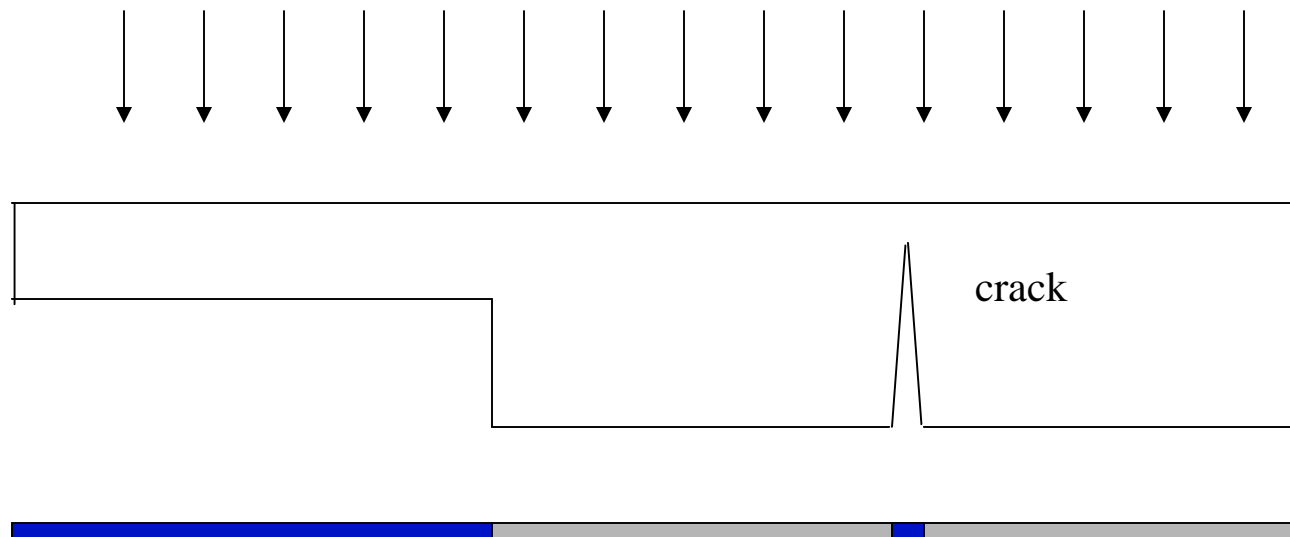
- Imaging technique similar to medical ultrasound
- Increasing in importance lately in nuclear NDE
 - Equipment is getting smaller, cheaper, and more powerful
 - Demands for speed are increasing
 - Cost
 - Low dose



Radiographic examination (RT)

- Principle

- Density changes on film or solid state detector caused by absorption differences in a component reveal internal features
- Volumetric method



Film image

Radiography

- Applicable to many components
- Radiological controls limit usefulness during intensive plant outage activities
 - Have to evacuate the area, disrupts other work
- Not sensitive to off-axis planar defects

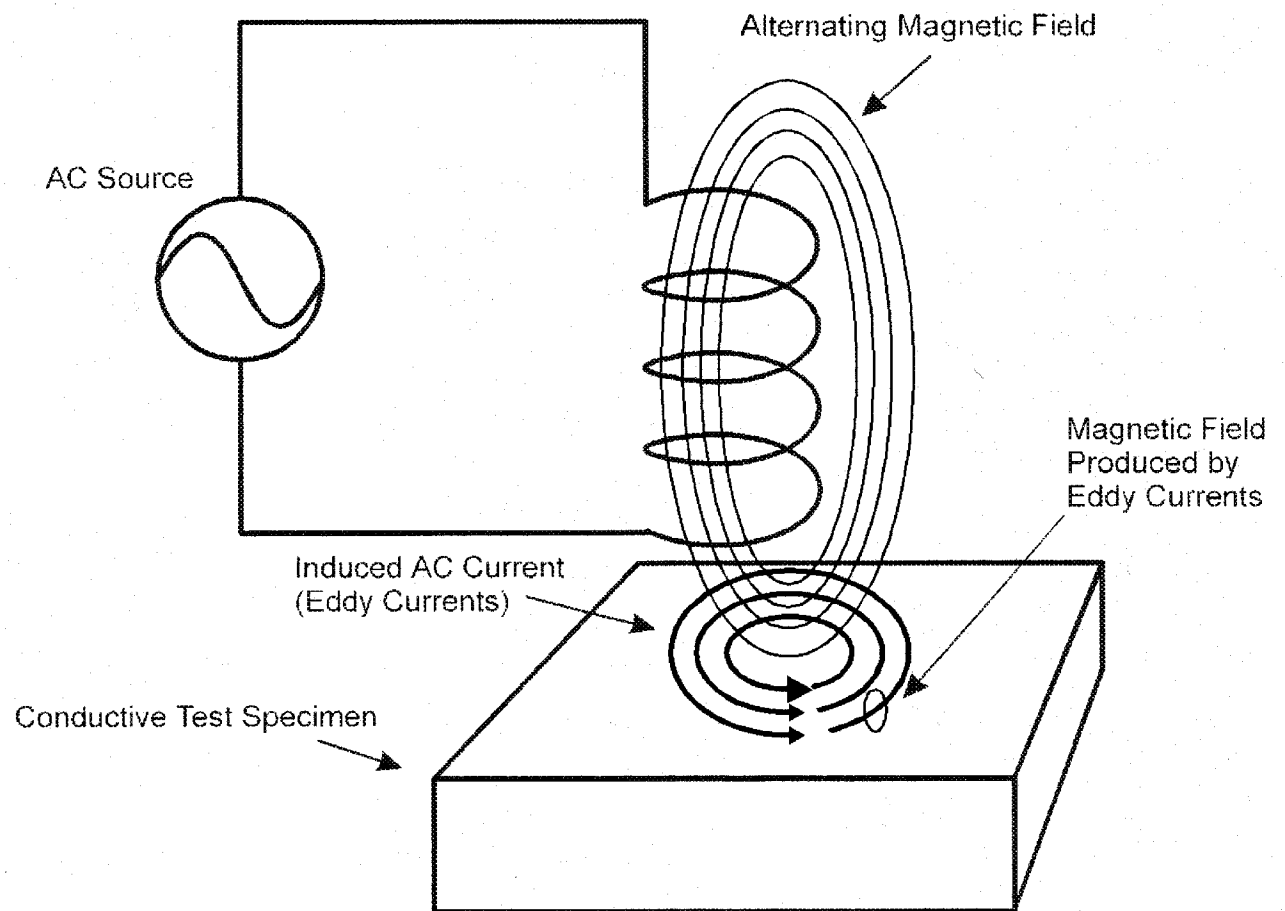
Eddy current examination (ET)

- Principle
 - Interaction of electromagnetic field with the material
 - Reveals surface and very near-surface features

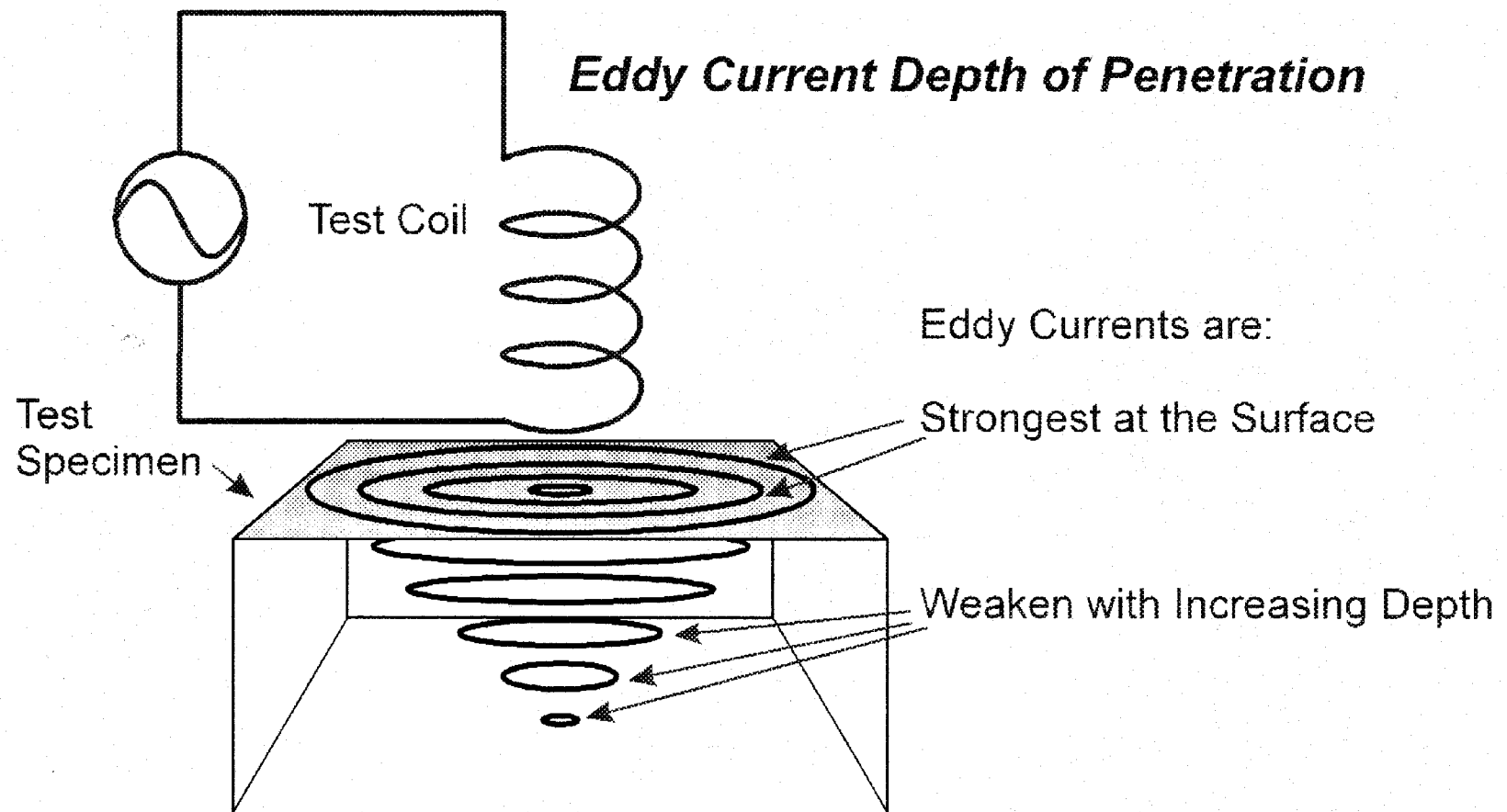
Eddy Current

- Principle

- Interaction of electromagnetic field with the material
- Reveals surface and very near-surface features



Eddy Current Principles



Liquid penetrant examination (PT)

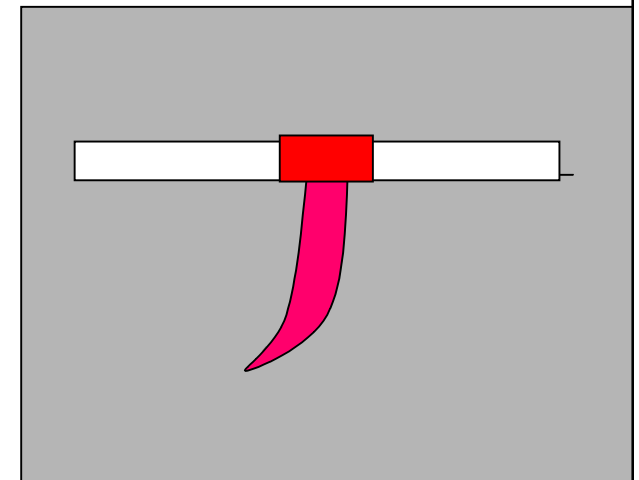
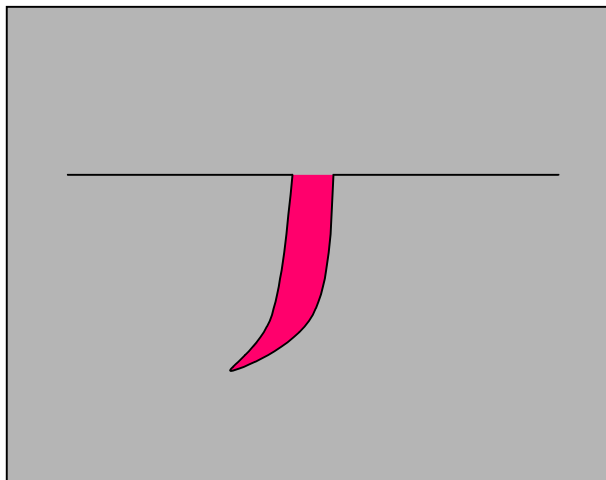
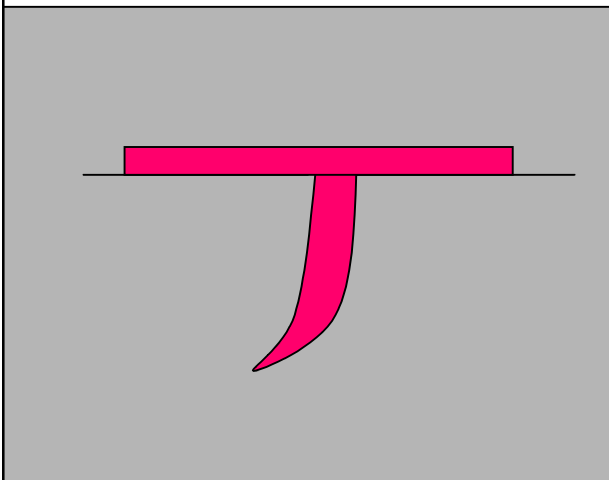
- Principle

- Indicator liquid (essentially, bright-red WD-40) drawn into surface breaking discontinuities by capillary action
- Indications revealed by developer (chalky spray)
- Strictly a surface examination method

Apply/dwell

clean

develop



Uncertainties

- Not all flaws that may be present will be detected
- location and sizing errors
- human errors
- NDE is only one part of the structural integrity picture
 - material properties
 - loads
 - environment

Other Reading

- Nondestructive Testing Handbook, ASNT, ISBN 0-931403-02-2
- ASM Handbook, Volume 17-Nondestructive Testing and Quality control, ISBN 0-87170-007-7
- Introduction to Phased Array Ultrasonic Technology Applications, RD Tech, Inc. ISBN 0-9735933-0-X
- Engineering Applications of Ultrasonic Time-of-flight Diffraction, JP Charlesworth and J.A.G. Temple, ISBN 0-86380-085-8

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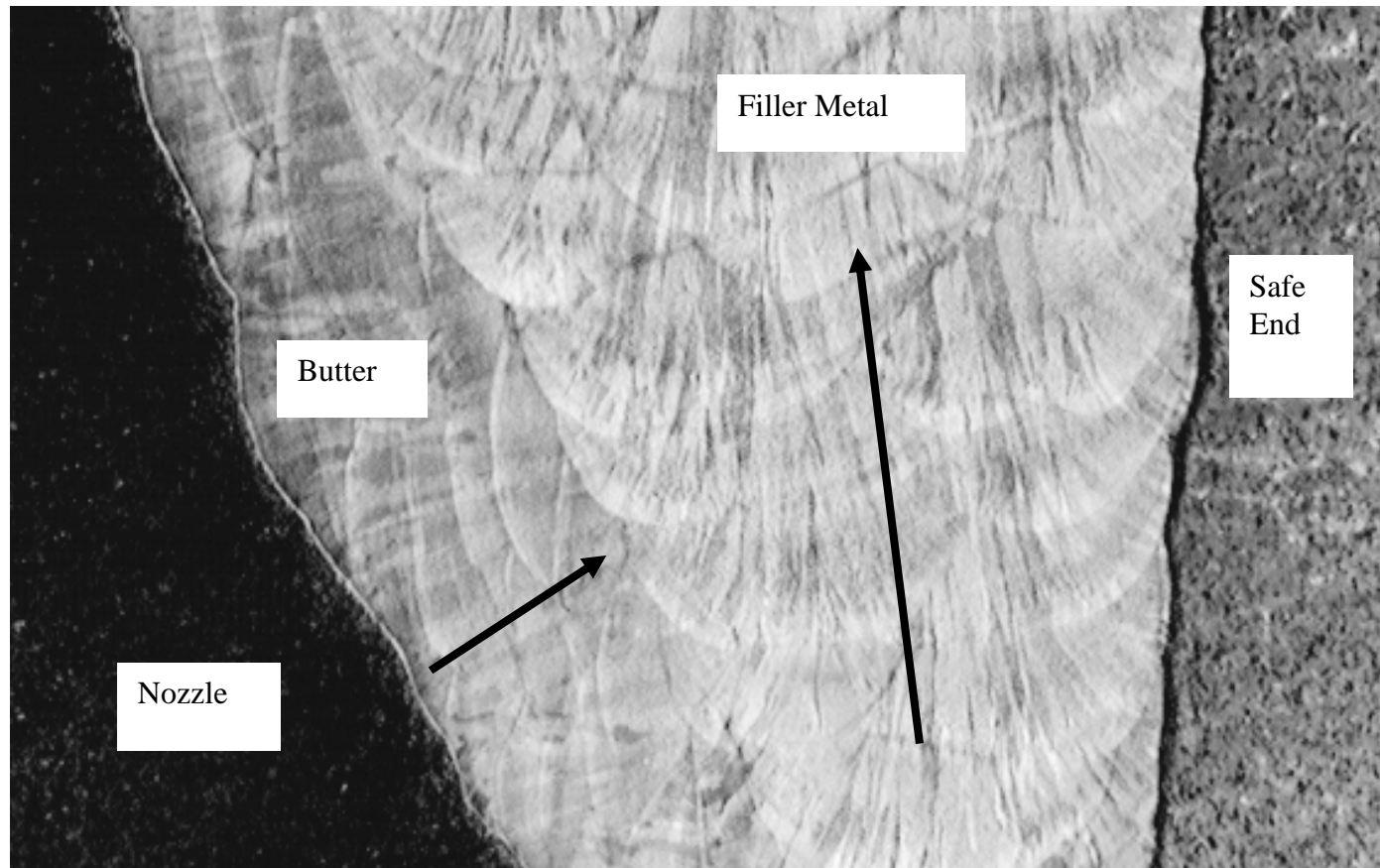
NDE of Stainless & Nickel Based Components

- Piping
 - Wrought and cast
 - Welds
 - Fittings
 - Elbows, Tees, etc
- Pump & valve bodies
- Vessel cladding & internals
- Vessel penetrations
- Steam generator and other heat exchanger tubing

UT of Stainless Steel and Nickel-based alloys

- UT is used extensively for volumetric inspection of SS & Ni based based piping welds
- Austenitic welds are acoustically anisotropic
 - Acoustic velocity is a function of beam direction with respect to the crystallographic orientation
- Each grain boundary is an impedance mismatch which causes
 - Attenuation (sensitivity loss)
 - Scattering
 - Noise
 - False calls
 - Interpretation errors
 - Re-direction of the beam can cause location errors and gaps in coverage

Dendritic Grain Structures in a Dissimilar Metal Weld

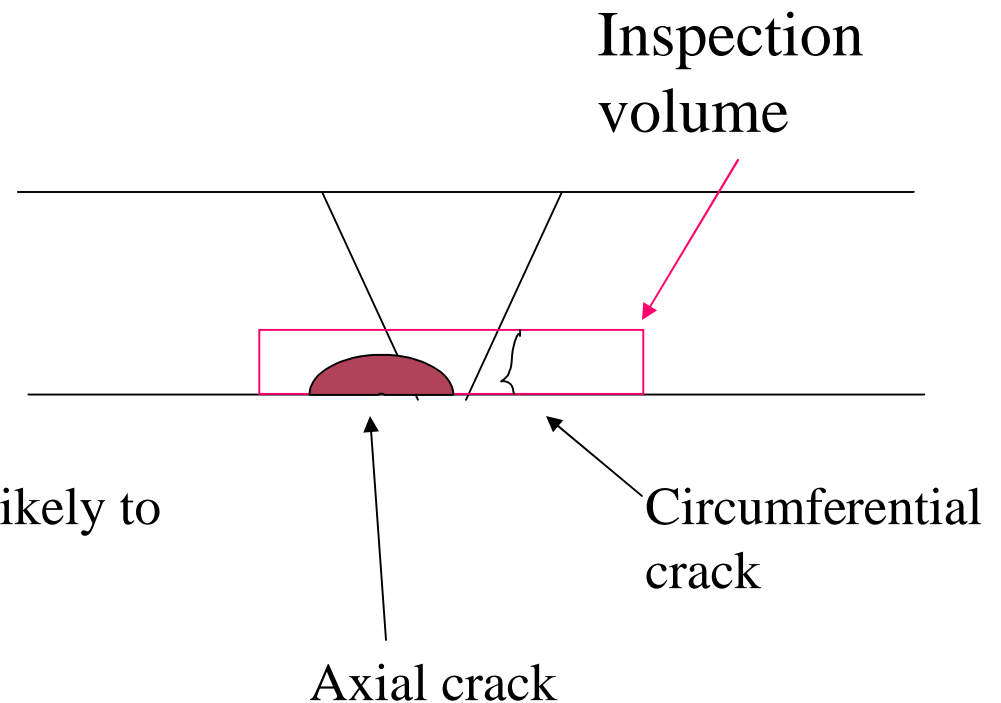


Piping Weld NDE

- Volumetric examination

Degradation mechanisms are most likely to initiate from the inside surface

- Stress corrosion cracking
- Flow assisted corrosion (FAC)
- Fatigue cracking
- Must consider the potential for axial or circumferential cracking



Intergranular stress corrosion cracking (IGSCC)

- Typically found in BWR SS piping welds and RPv internals sensitized to SCC
- Primary location is weld heat affected zone (HAZ)
 - Crack typically starts near the weld root
 - Progresses through the wall following the HAZ

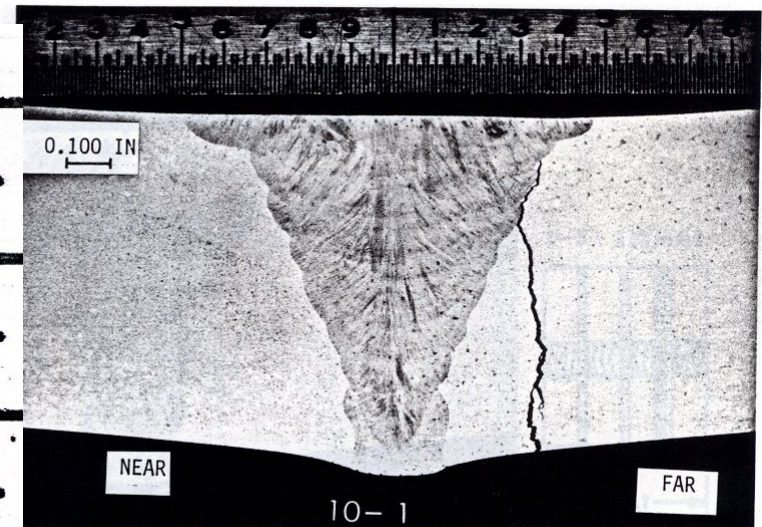
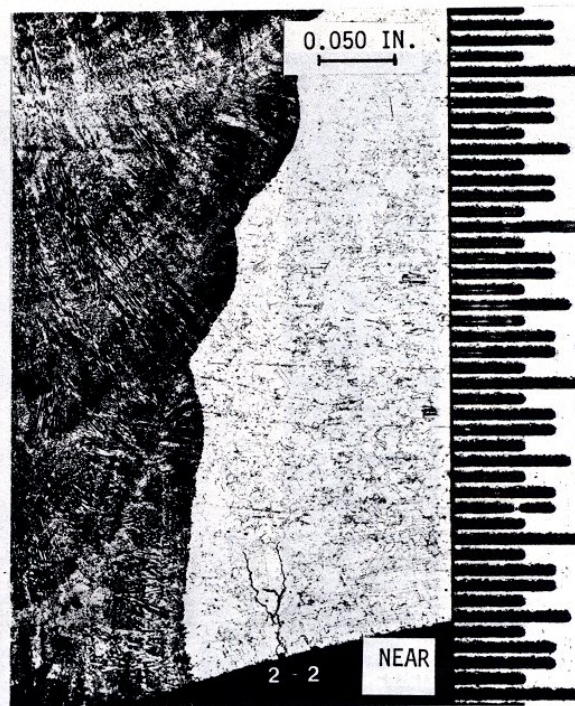
BWR Recirculation Piping-IGSCC

Typical IGSCC found in stainless steel BWR recirculation system piping

- Located in Heat Affected Zone of base metal
- Branched

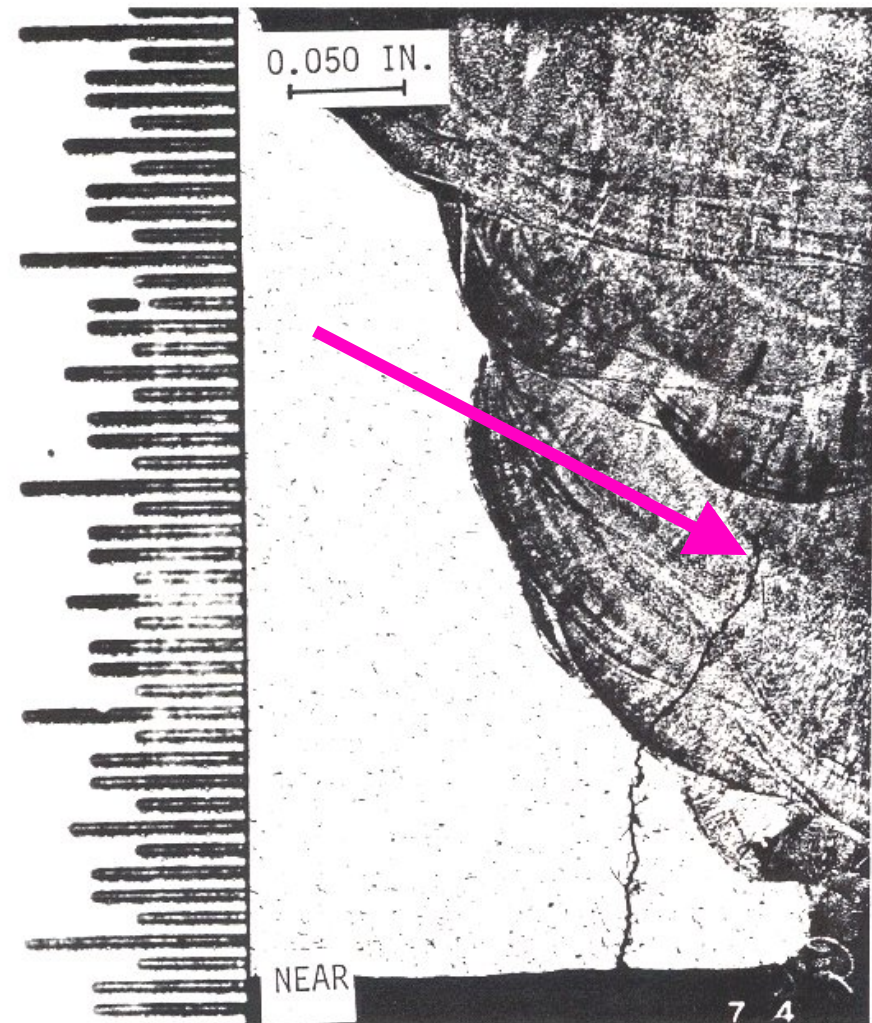
Example of deep cracking

- Grows toward weld
- Usually follows weld profile after reaching the weld



BWR Recirculation Piping-IGSCC

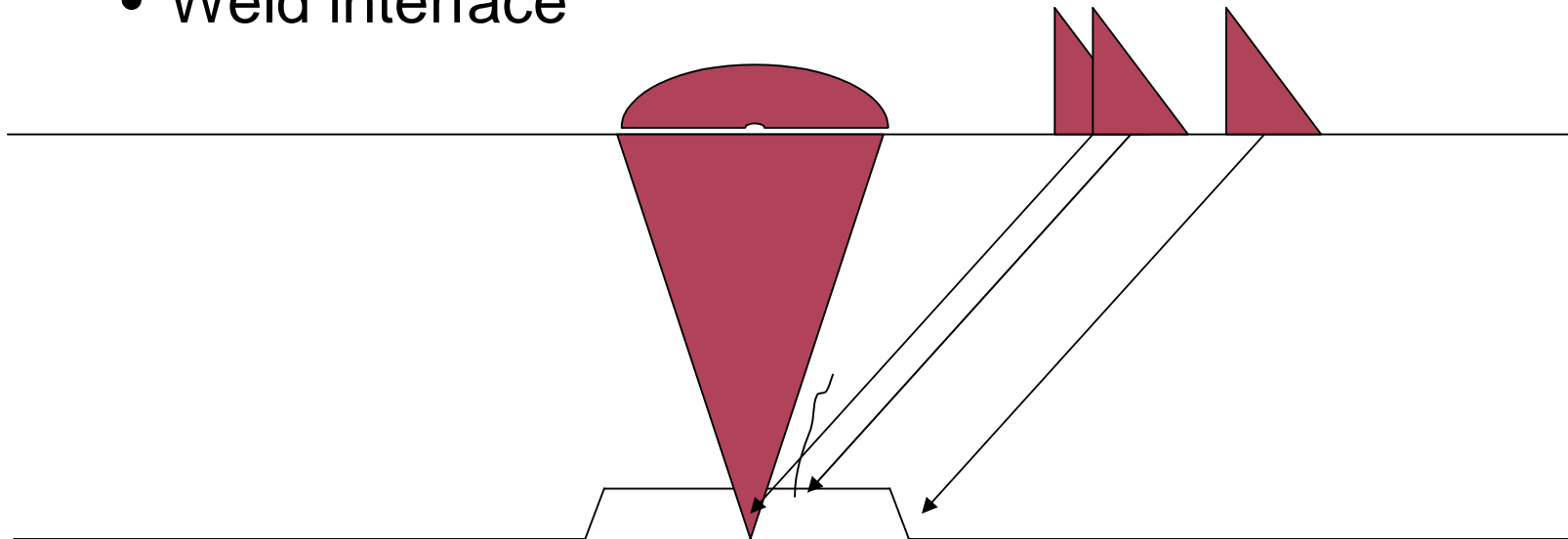
Example of crack growing into weld



IGSCC Discrimination

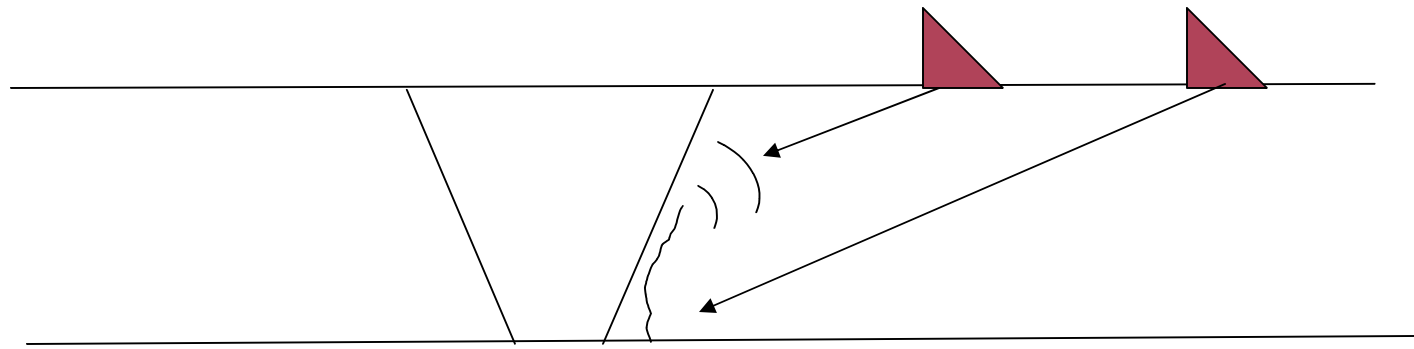
Root, Flaw, Counterbore

- UT crack detection
 - Identification of the crack signal is challenging when there are other competing signals
 - Weld root
 - Counterbore
 - Weld interface



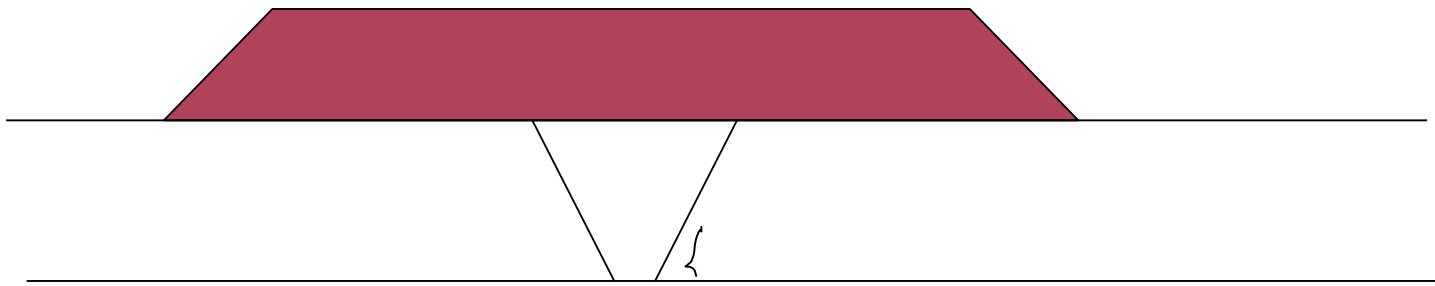
IGSCC

- Sizing is very challenging
 - Locating a diffracted wave from the crack tip
 - Difference in time-of-flight between the crack base and crack tip is used to calculate the depth
 - Experience needed to identify the tip signal



Overlay Repair

- Application of weld overlay is an effective repair method for cracked piping
 - Restores full structural integrity to a cracked pipe
 - Prevents further crack initiation and growth
- Requires good inspection after application, and continued monitoring
 - Verify integrity of the overlay itself
 - Monitor to ensure no growth of original cracks



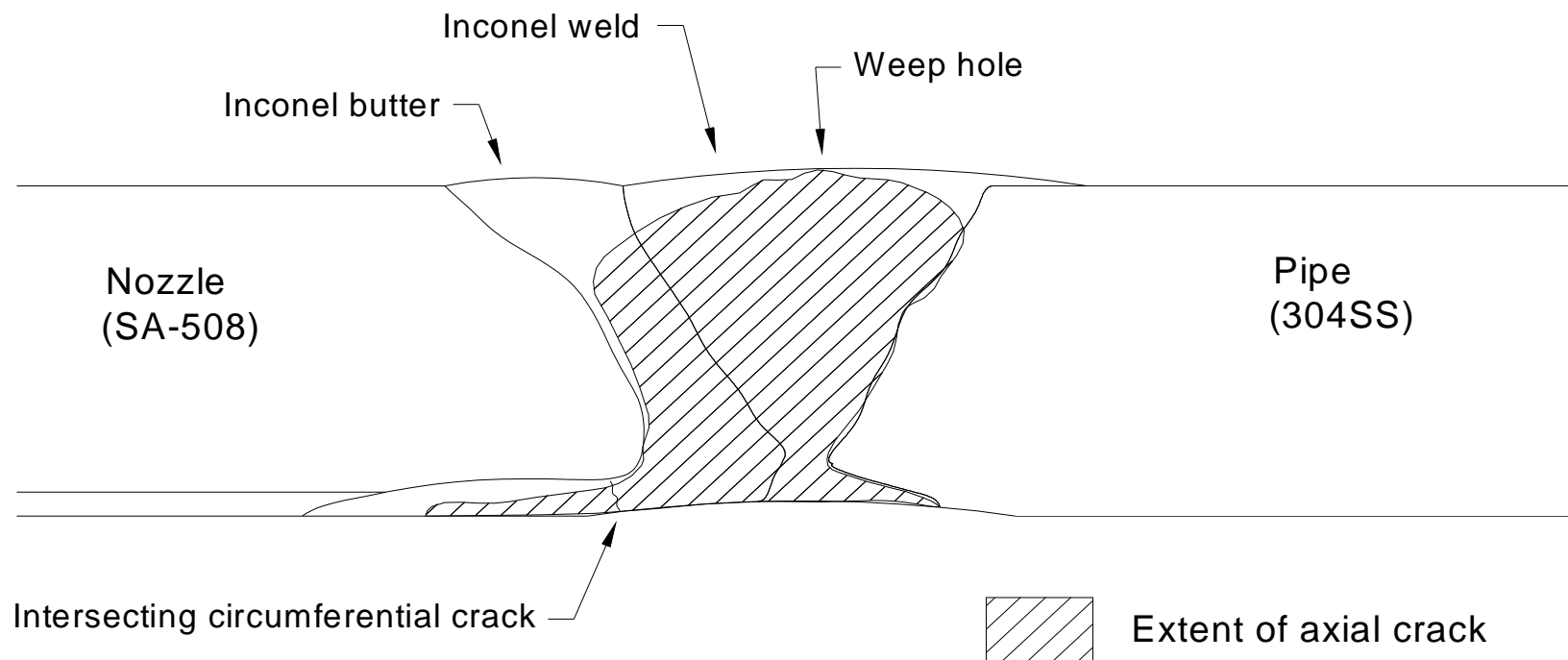
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Primary water stress corrosion cracking (PWSCC) in PWR Units

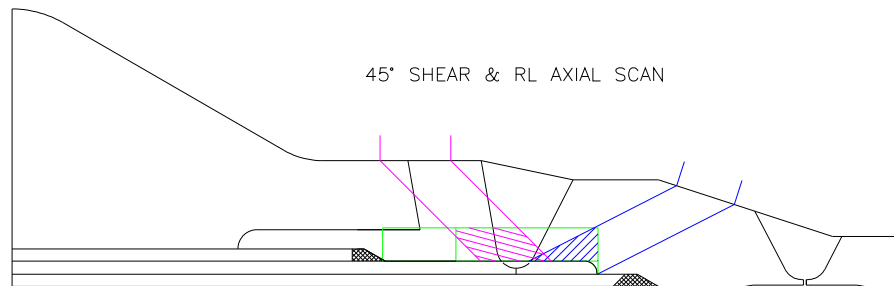
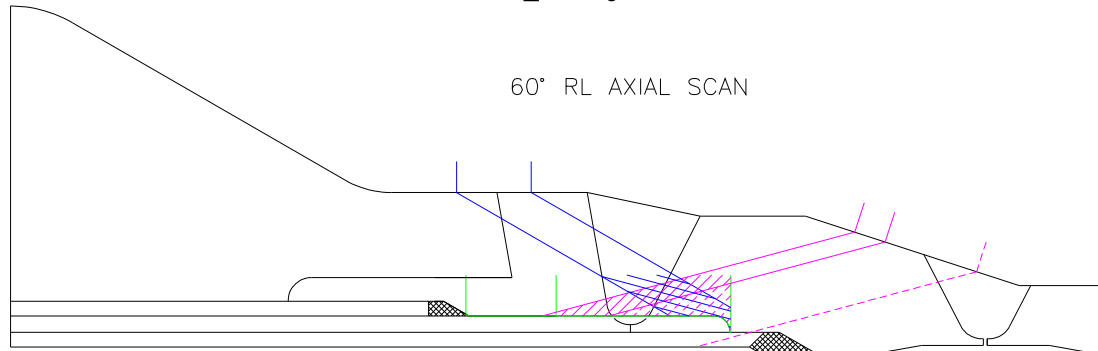
- PWSCC has been found in PWR main coolant systems with Alloy 600/182/82
- Alloy 182 welds
 - Dissimilar metal (DM) piping welds
 - Vessel head penetrations
- Alloy 600
 - Steam generator tubing

PWSCC in PWR Nozzle-Safe End Dissimilar Metal Weld at VC Summer Plant



Examination of Dissimilar Metal Welds

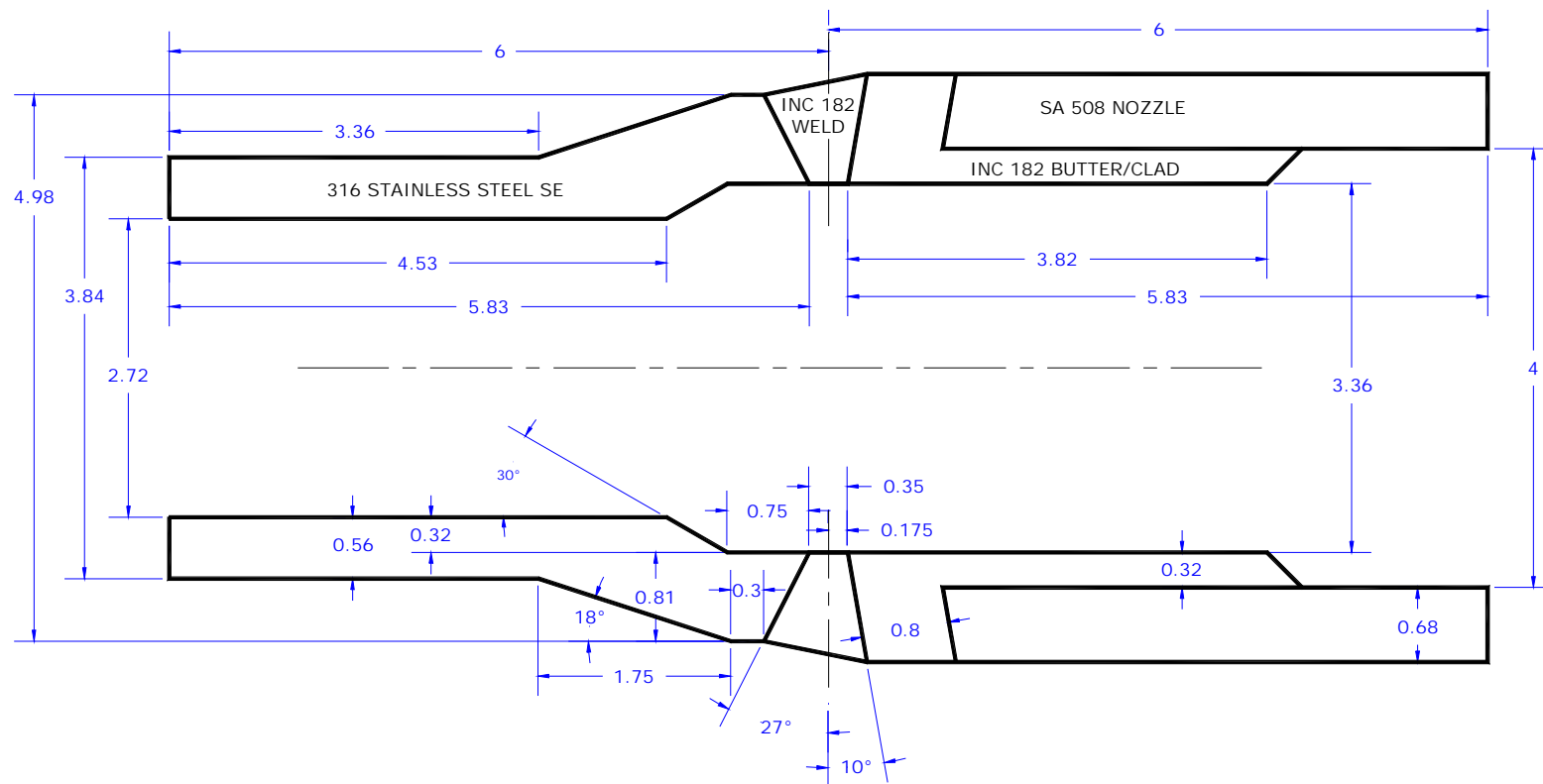
Pressurizer Spray/Relief nozzles



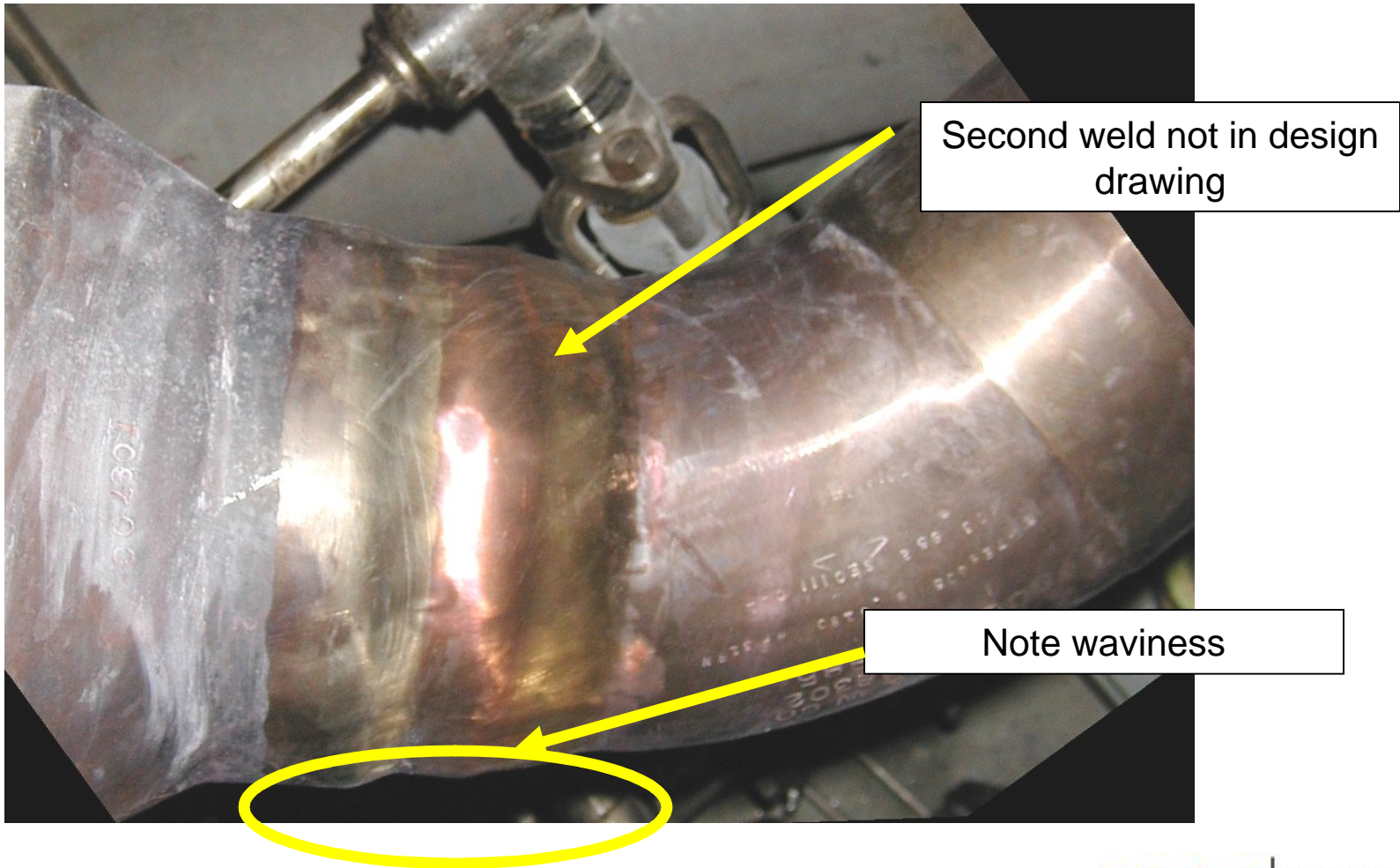
Must use a combination of probe angles and scanning surfaces to obtain coverage of the examination volume-**may not get all of it**

Design Drawings can't be trusted

PWR PRESSURIZER SPRAY NOZZLE CONFIGURATION (704/X)



Actual Configuration



Example of a PWSCC Issue

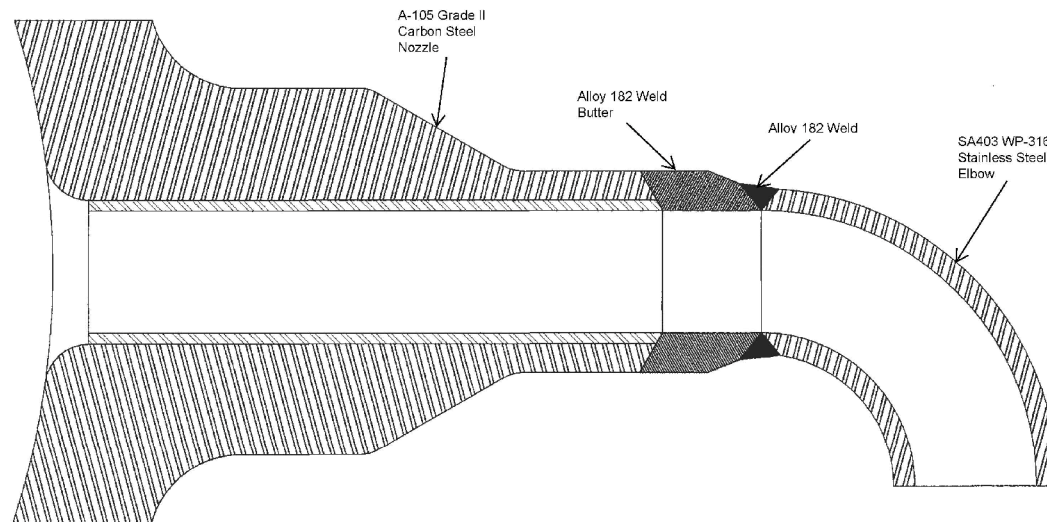
- Indication detected in a PWR cold leg drain line dissimilar metal weld
- Evaluated as a defect
- Overlay repair designed and installed

RCP 1-1 Cold Leg Drain

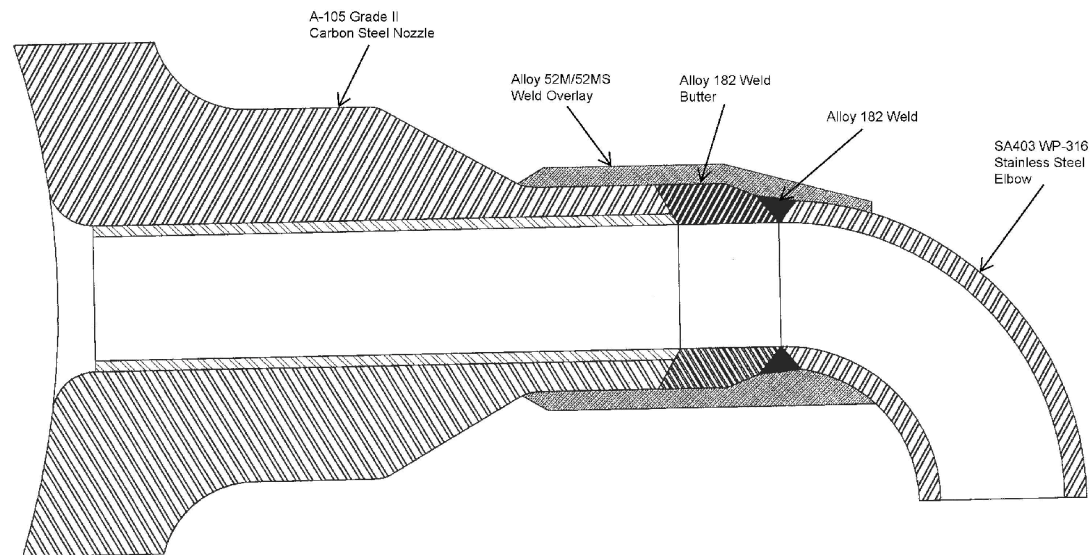


RCP 1-1 Cold Leg Drain

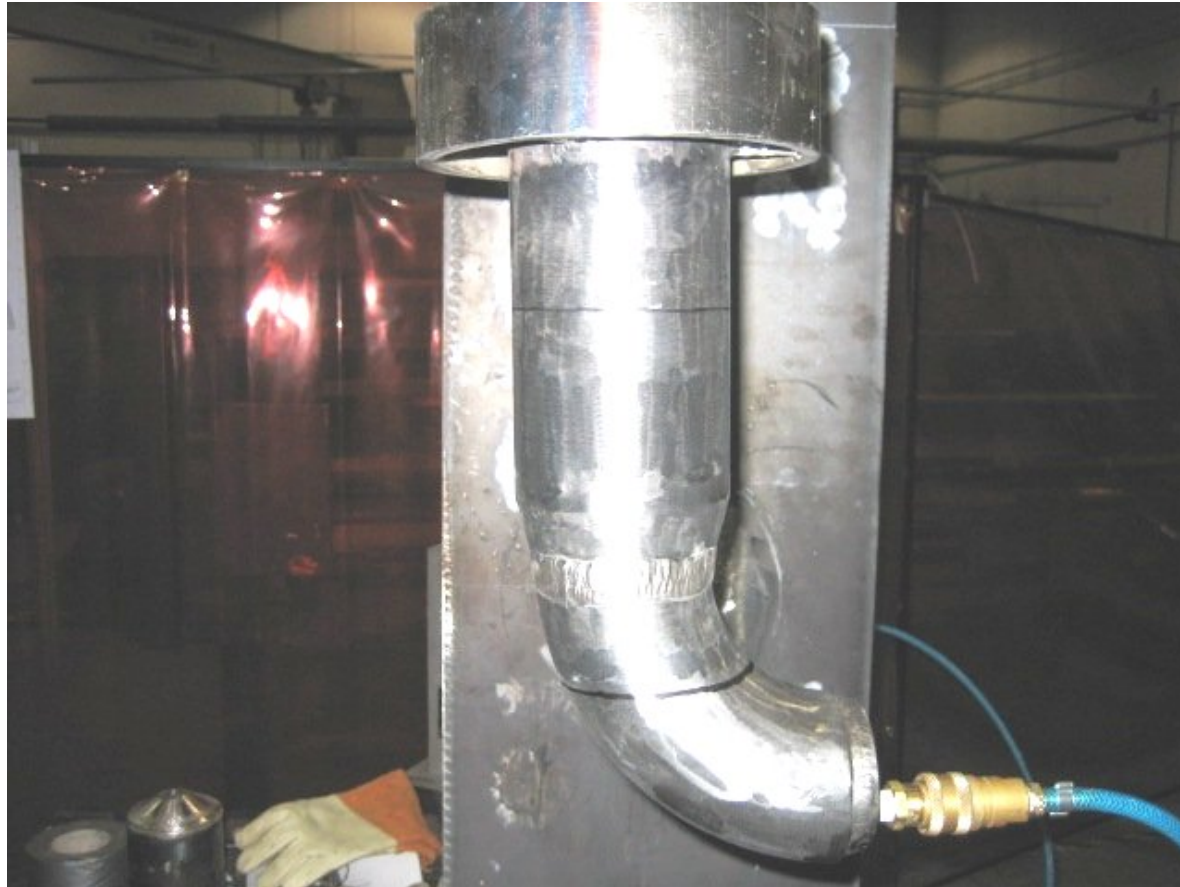
As-built configuration



Overlay configuration



RCP 1-1 Cold Leg Drain



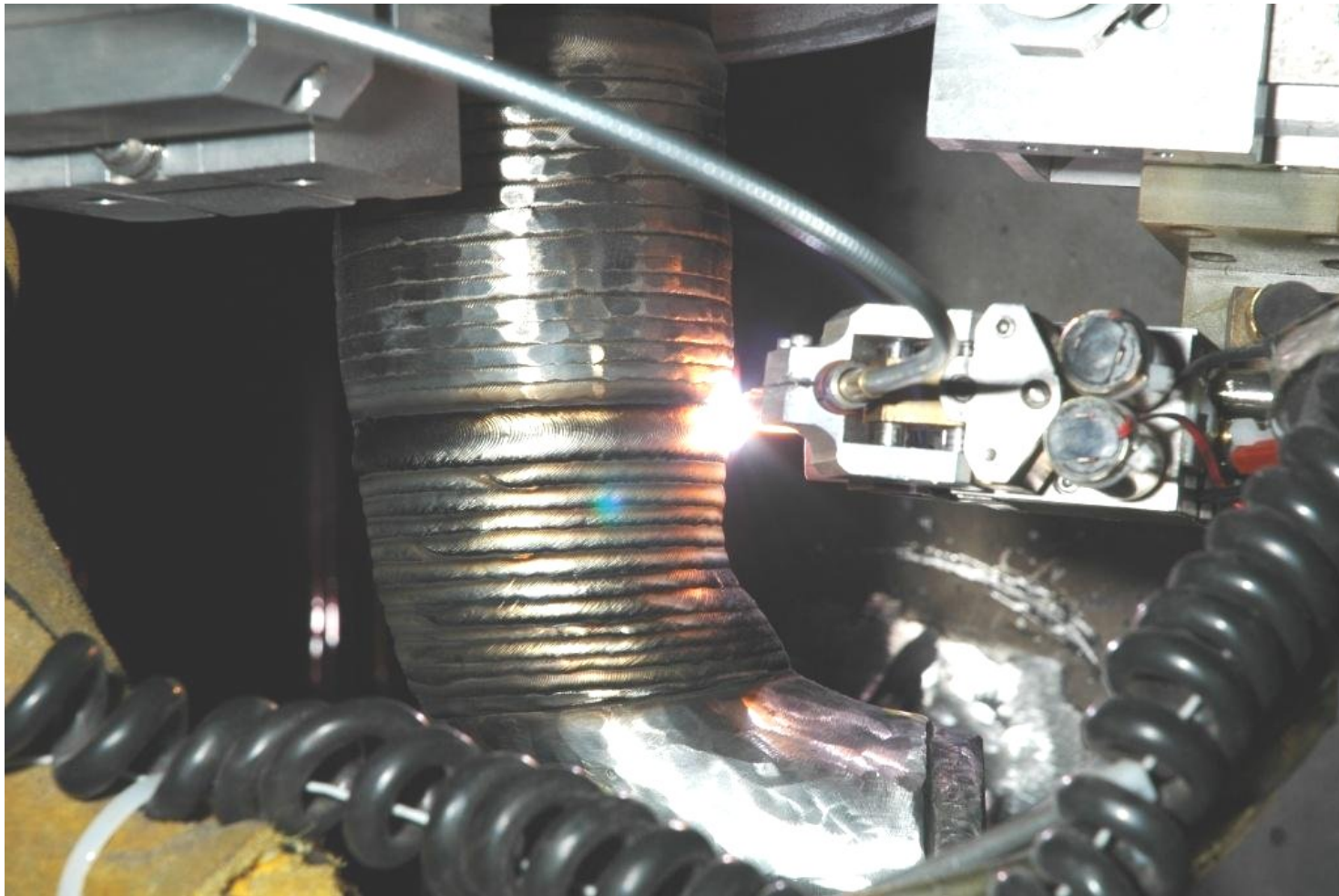
Mockup for Welding Proof of Principle
WSI Norcross, GA

RCP 1-1 Cold Leg Drain



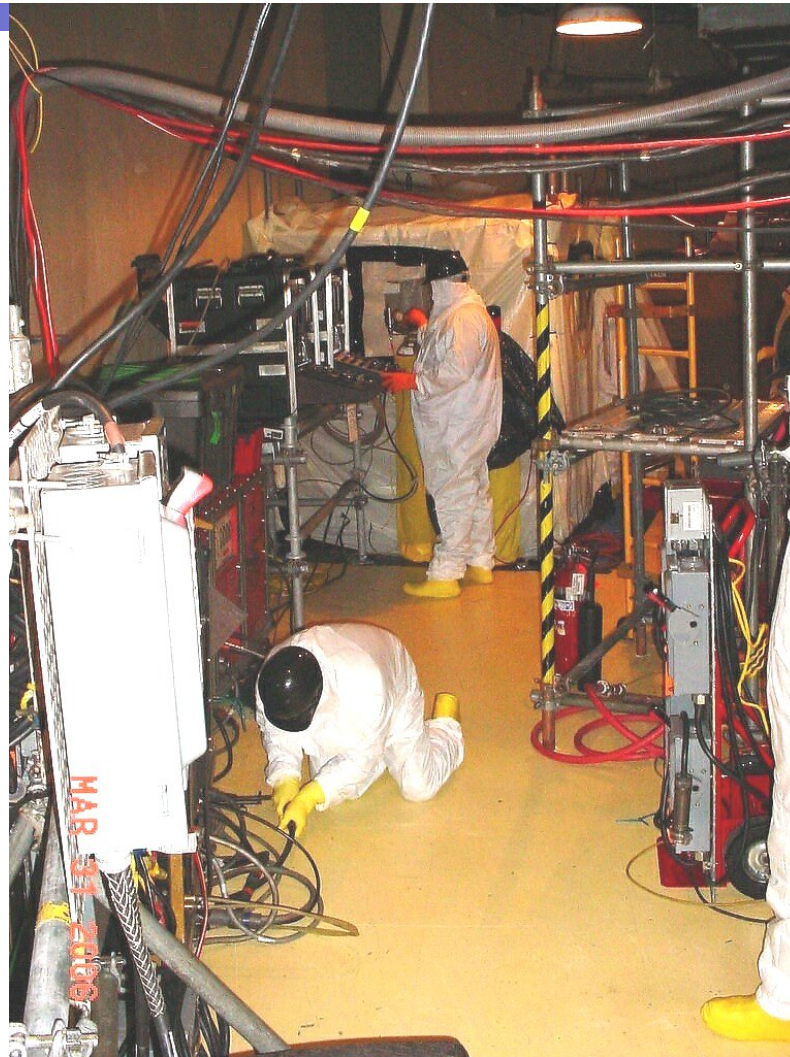
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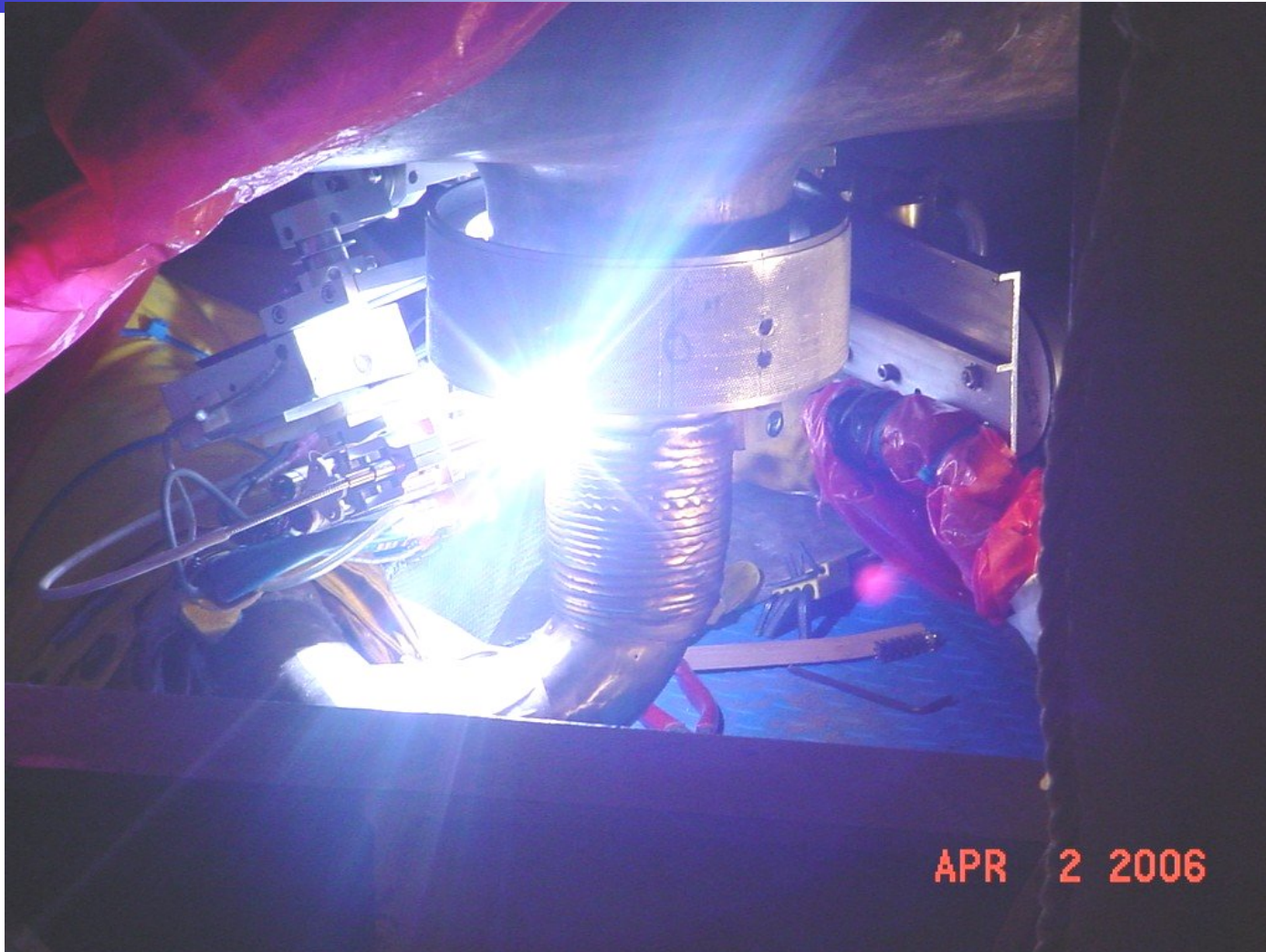
WSI Welding Power & Controls Setup

RCP 1-1 Cold Leg Drain



WSI Remote Welding Operation

RCP 1-1 Cold Leg Drain



Welding the Overlay – Day 15 After Indication Discovery

RCP 1-1 Cold Leg Drain



Final UT'd Overlay – 16 Days 6 Hours After Indication Discovery

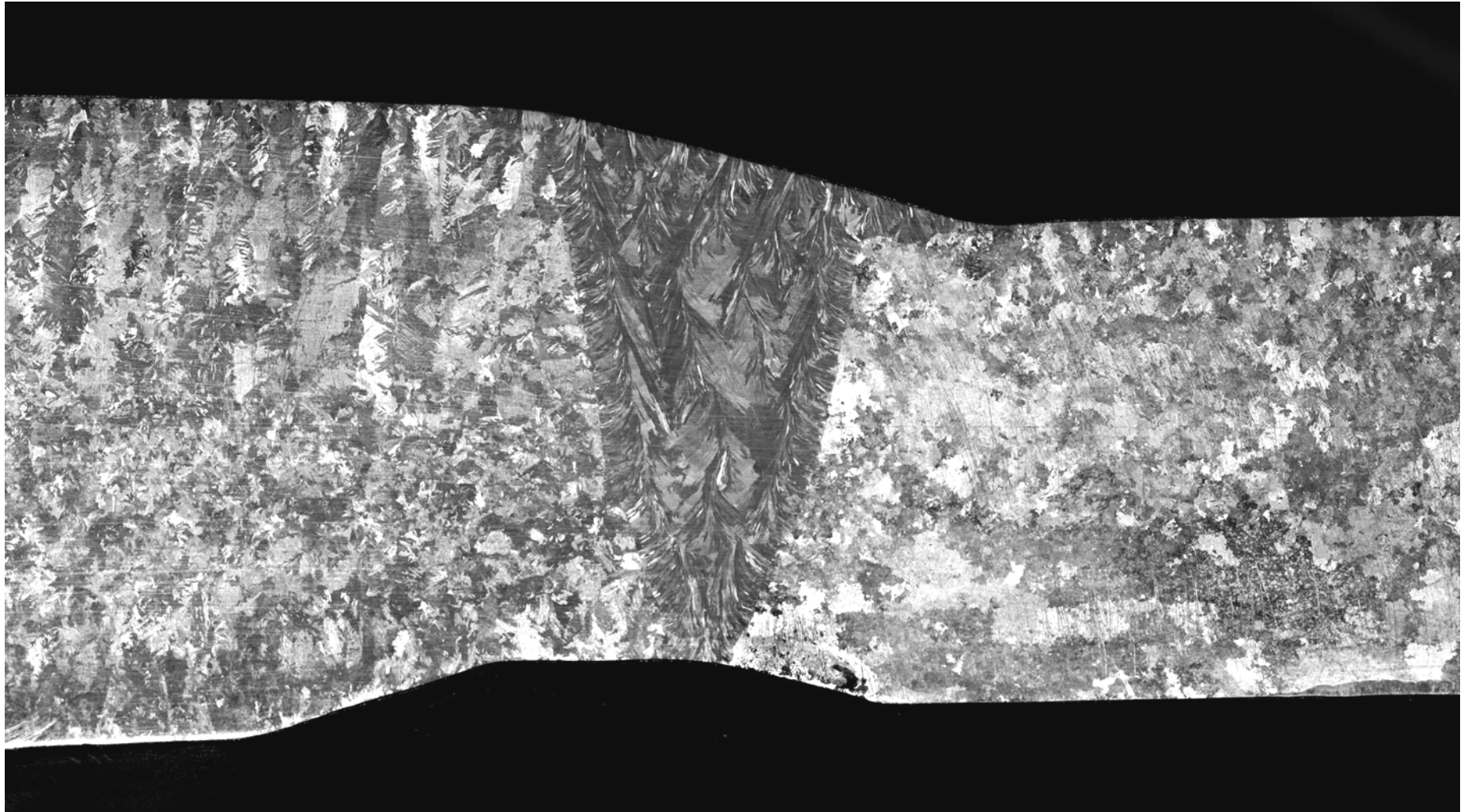
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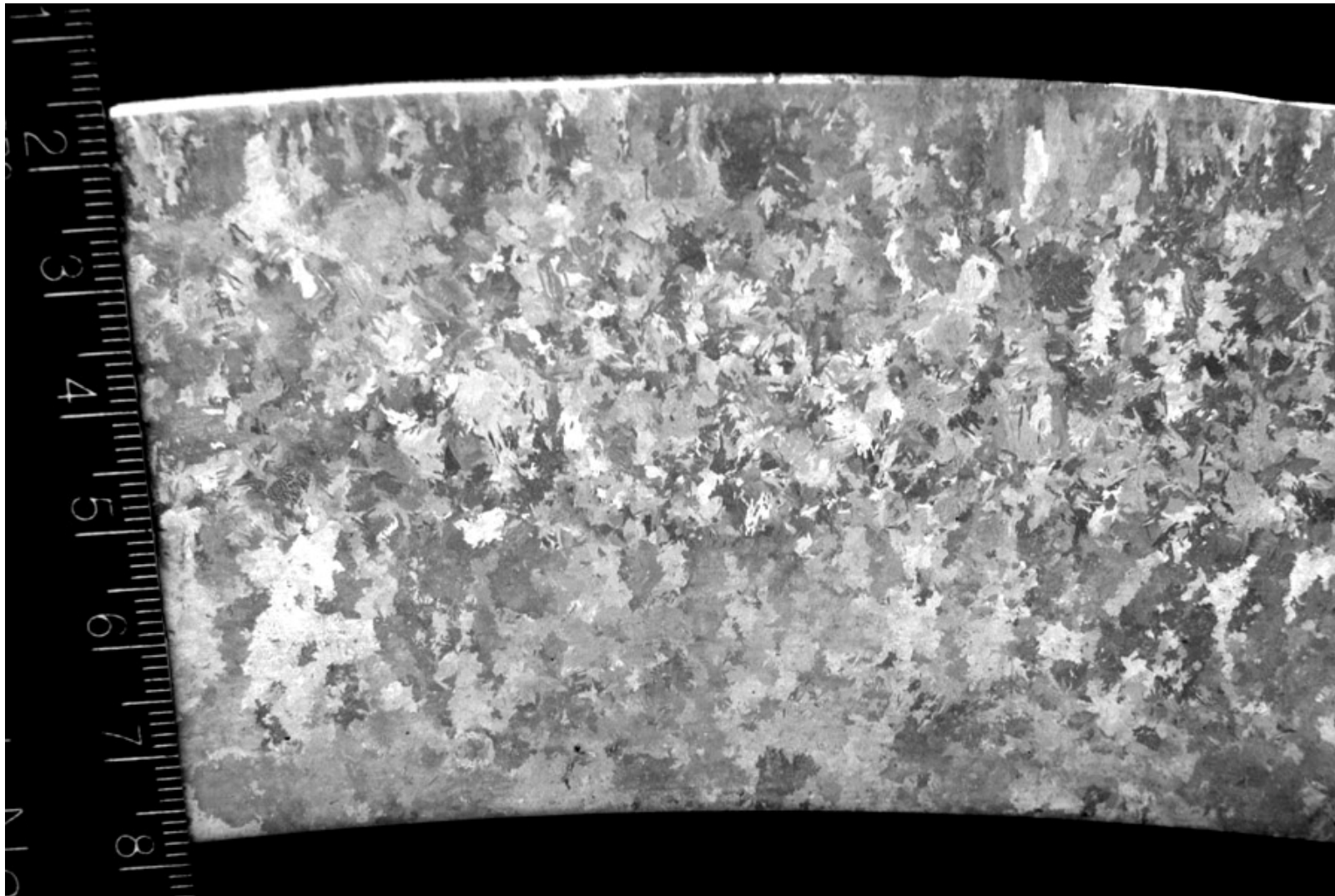
Cast Stainless Steel

- Some components are stainless steel castings
 - Pump and valve bodies, piping elbows: statically cast
 - Piping: centrifugally cast
- Castings can have very large grains
- In stainless steel, this makes UT extremely difficult because the grains are acoustically anisotropic
- Only very low-frequency sound can penetrate the metal
 - Poor resolution
 - Possibility of transmission through the face of a tight crack – no reflection, no detection
- Round-robin tests have shown that the UT capability is very poor (scanning on the outside, to detect cracking on the inside)

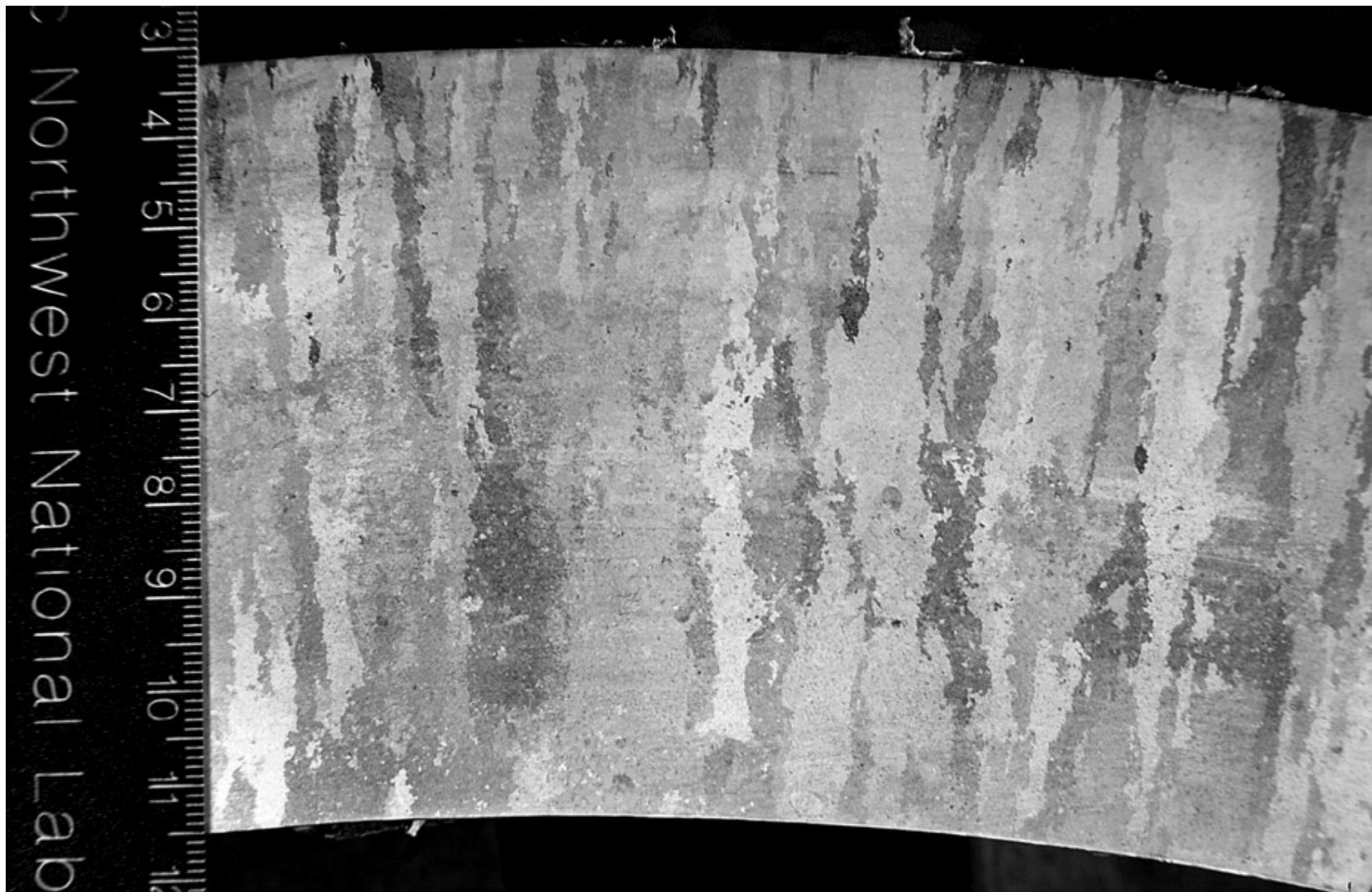
Cast Stainless Steel



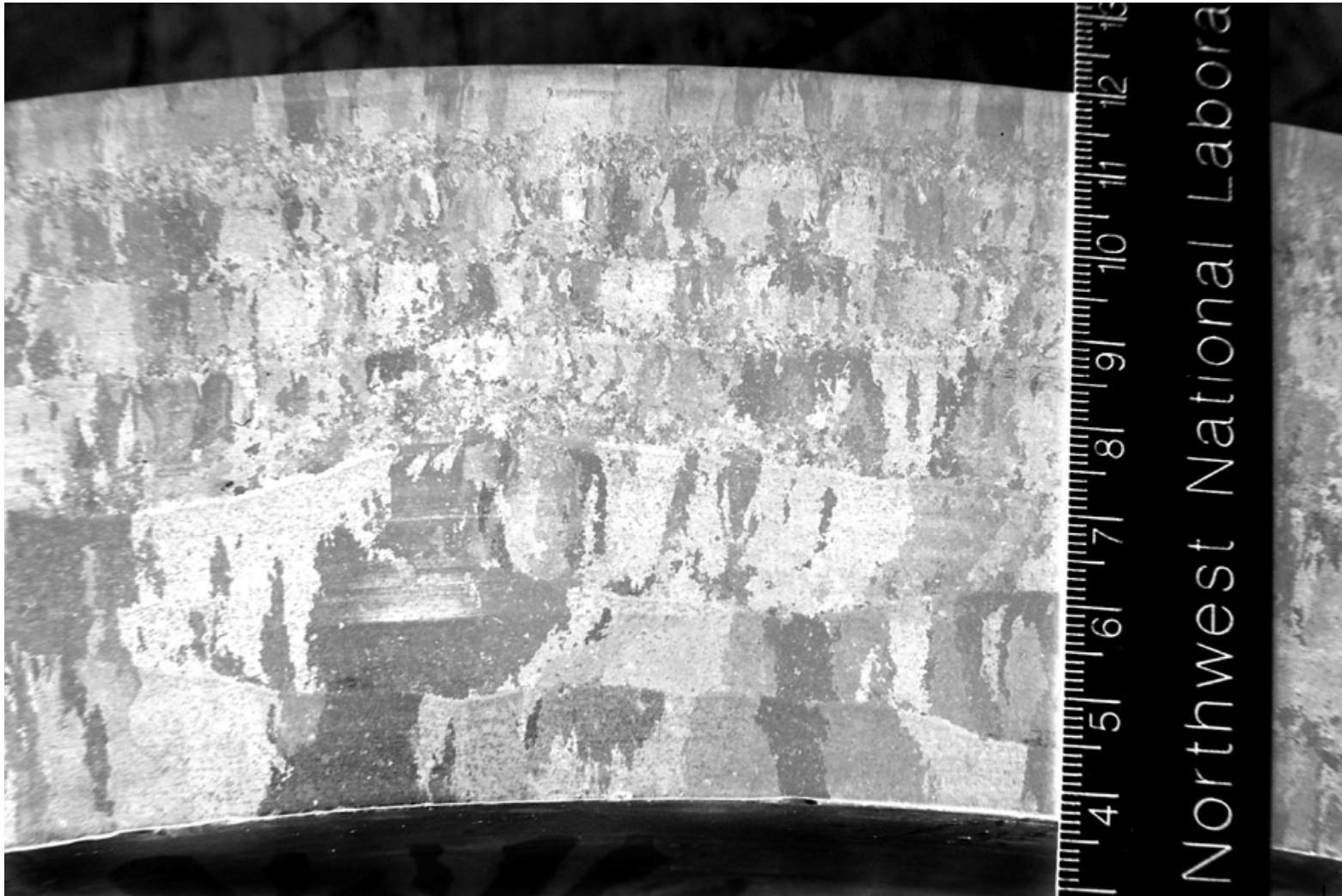
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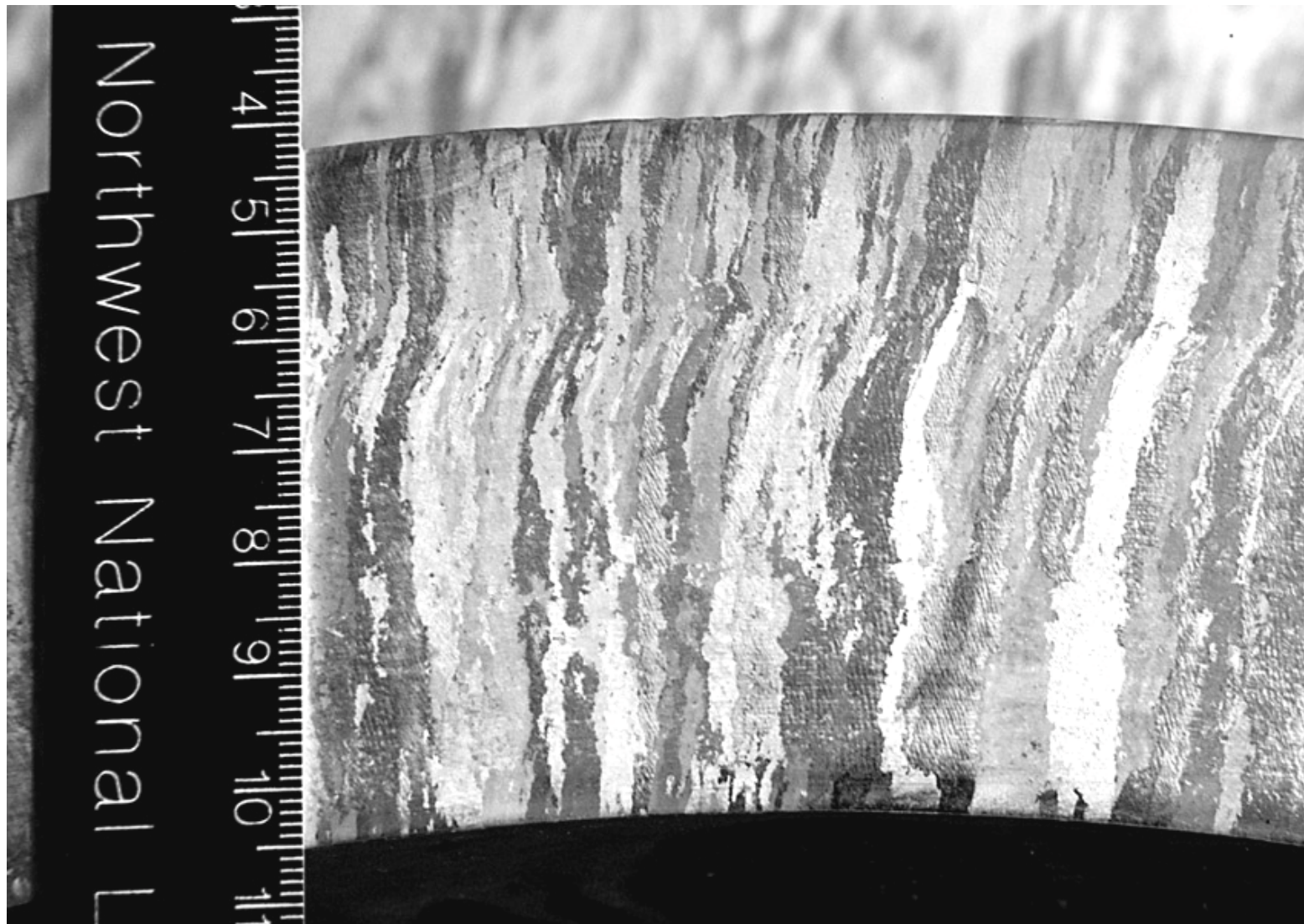
Cast Stainless Steel



Cast Stainless Steel



Cast Stainless Steel



Cast Stainless Steel

- No known degradation mechanism for CSS reactor coolant piping
 - No leaks
 - No failures
- No effective outside-surface UT technique is on the horizon
- Interest is growing
 - Thermal aging embrittlement
 - License renewal commitments
- Any significant effort to develop and qualify NDE will require fabrication of piping to use for mockups

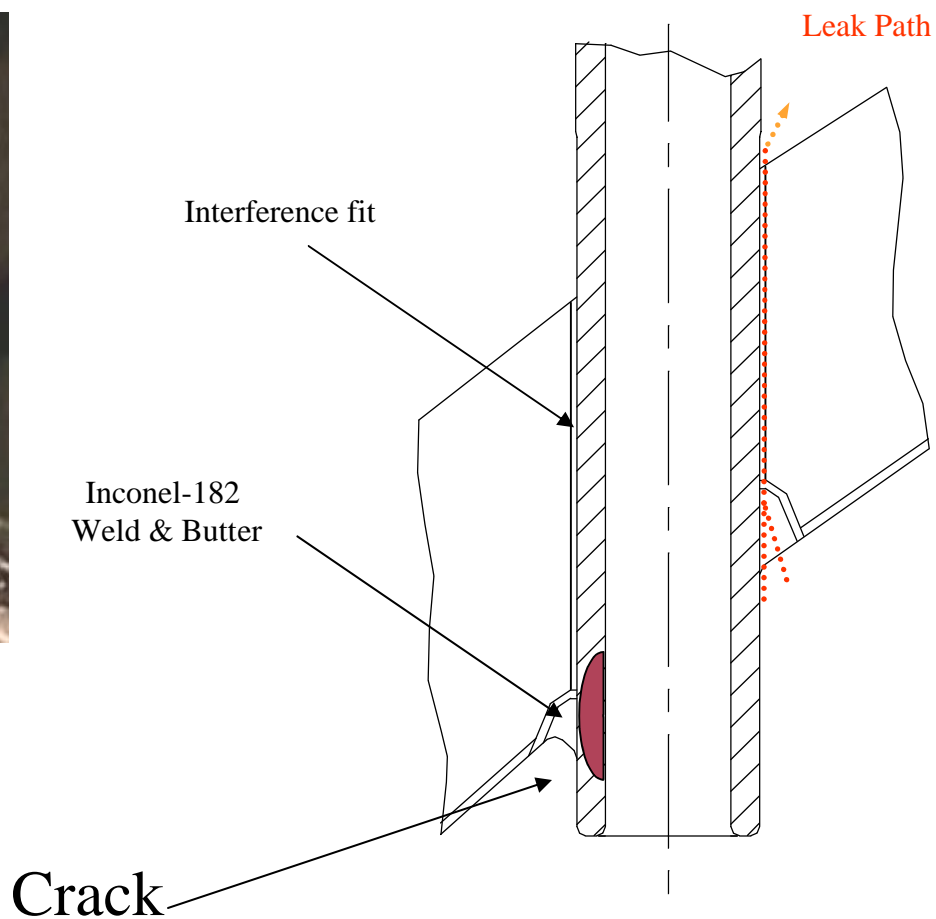
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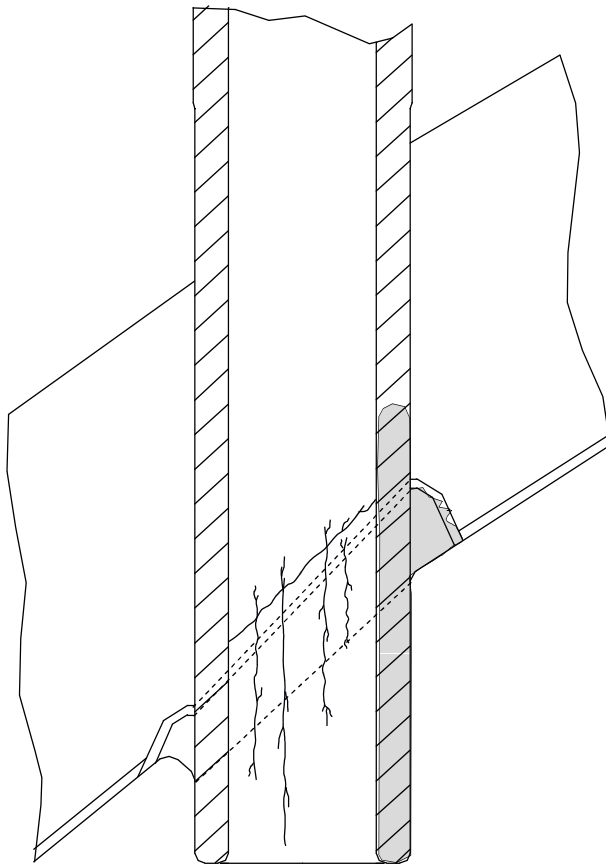
CRDM Penetration Leaks



Boric Acid deposits
on Top Head

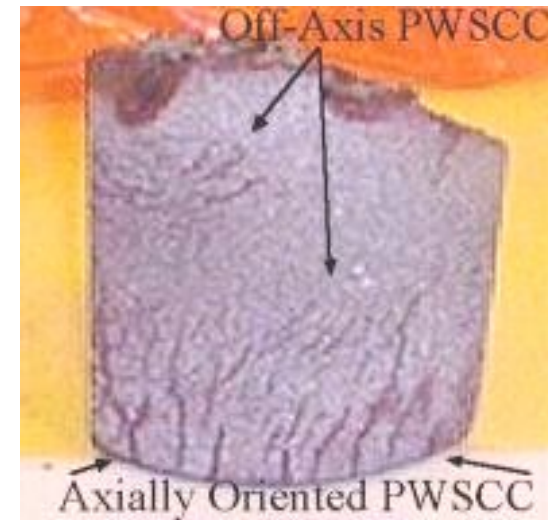


PWSSC in CRDM Penetrations



Base metal
PWSSC

J-Groove weld
cracking

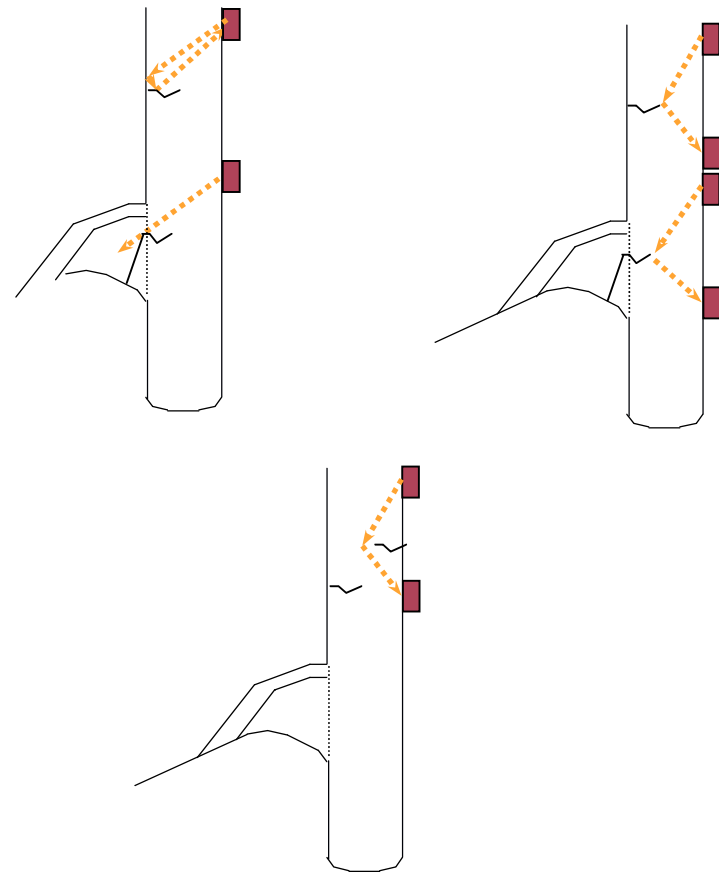


Evidence of Leakage

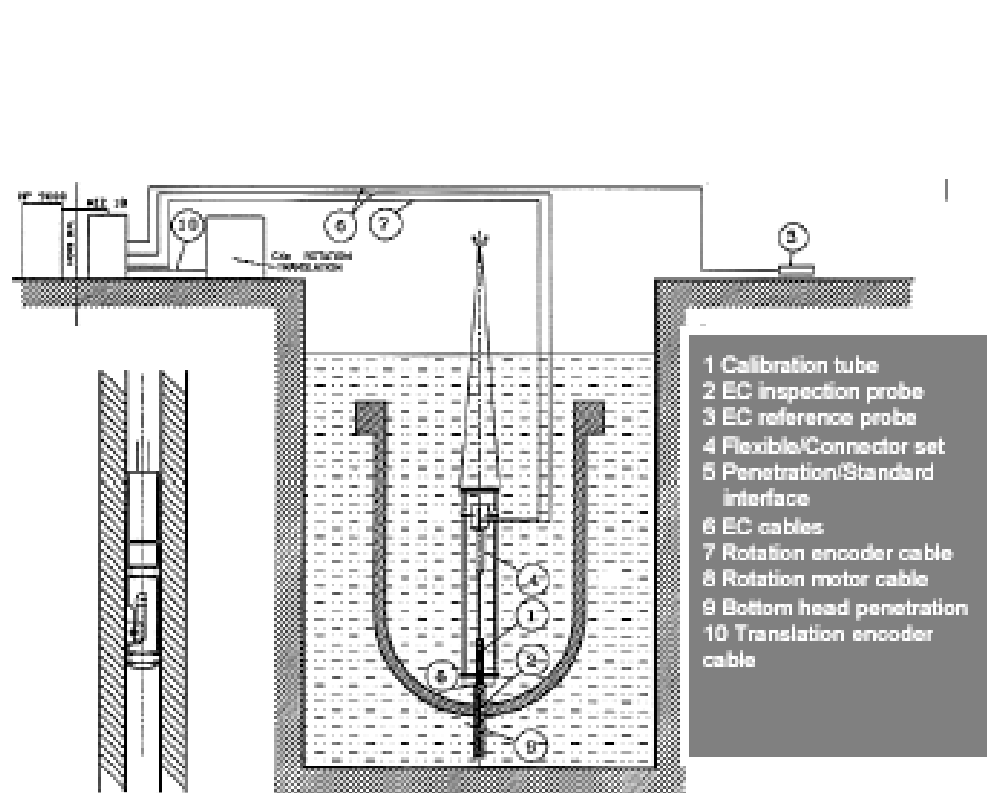


Inspection of Vessel Penetrations

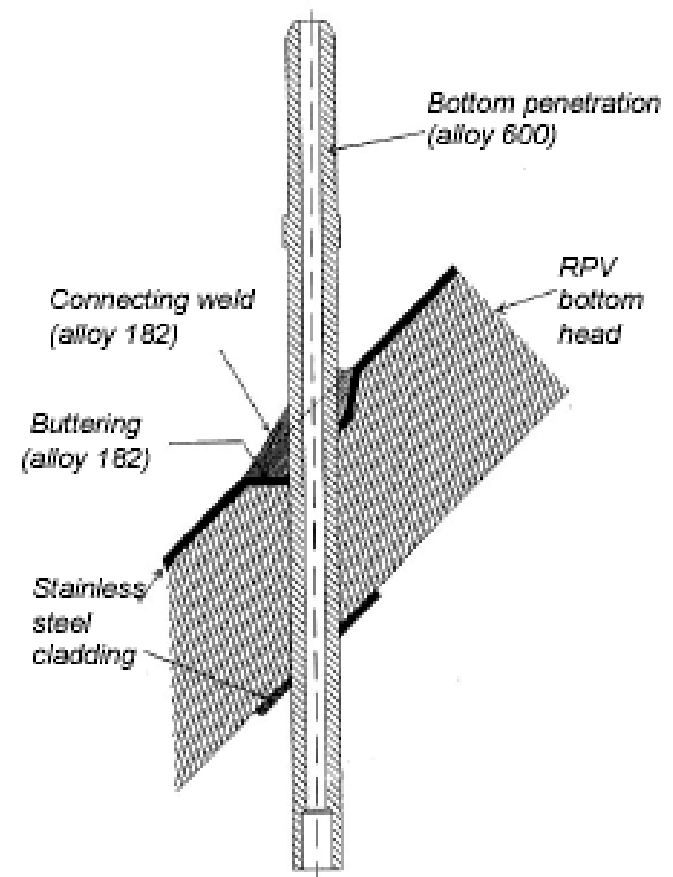
- UT used for detection and sizing
- ET is used in some cases for detection and length sizing
- ET used for surface examination of the wetted surfaces
- UT of the J-Groove weld has not been proven reliable-many sources of false calls



Bottom Mounted Instrumentation Penetrations



General Layout



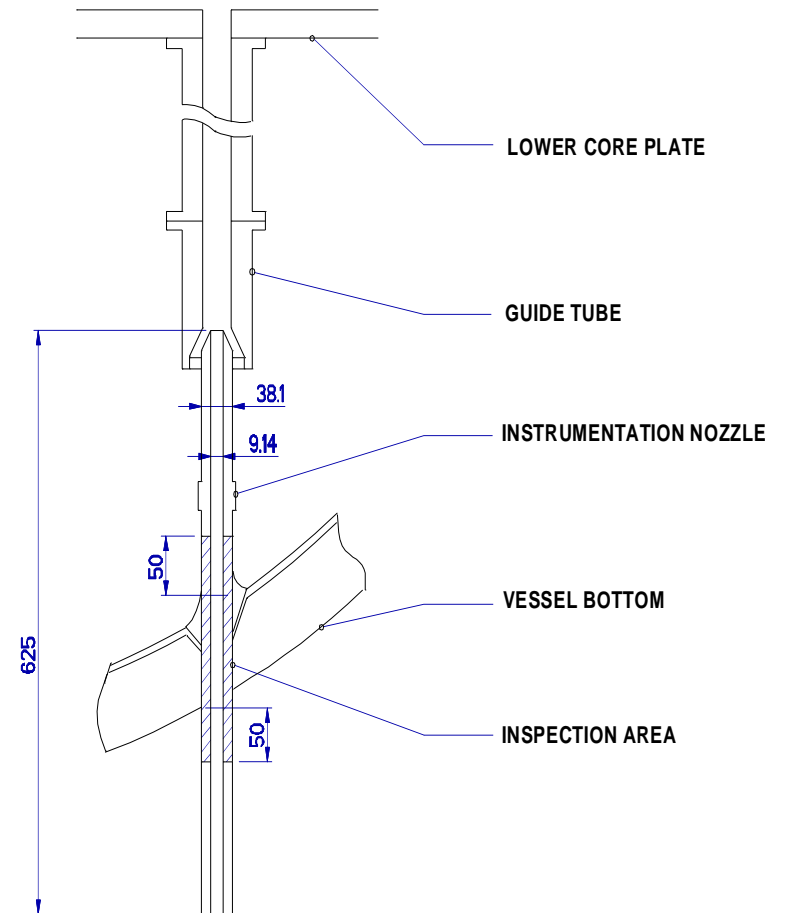
Bottom Mounted Instrumentation Penetrations

- Small amount of residue discovered on 2 BMI penetrations at South Texas Plant Unit 1
- Deposits confirmed to be boric acid from reactor coolant
- Very small amount of deposits- 150 mg and 3 mg



Bottom Mounted Instrumentation Penetrations

- Inspection approach under consideration
 - Volumetric examination of the tube
 - Surface examination of the J-groove weld
- Demonstration of techniques using mockups



Summary

- Inspection of stainless steel and Nickel based materials presents challenges
 - Anisotropy
 - Geometry
 - Access
 - High radiation areas
- Many of these problems can be overcome with proper advance knowledge of the configurations
 - Allow time for planning, training, and qualification of the process
- Gaps in the NDE technology remain
 - Welds with excessively wavy surfaces
 - Cast stainless steel
 - Volumetric examination of the J-groove welds in vessel head penetrations

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Pressure Vessel Inspection

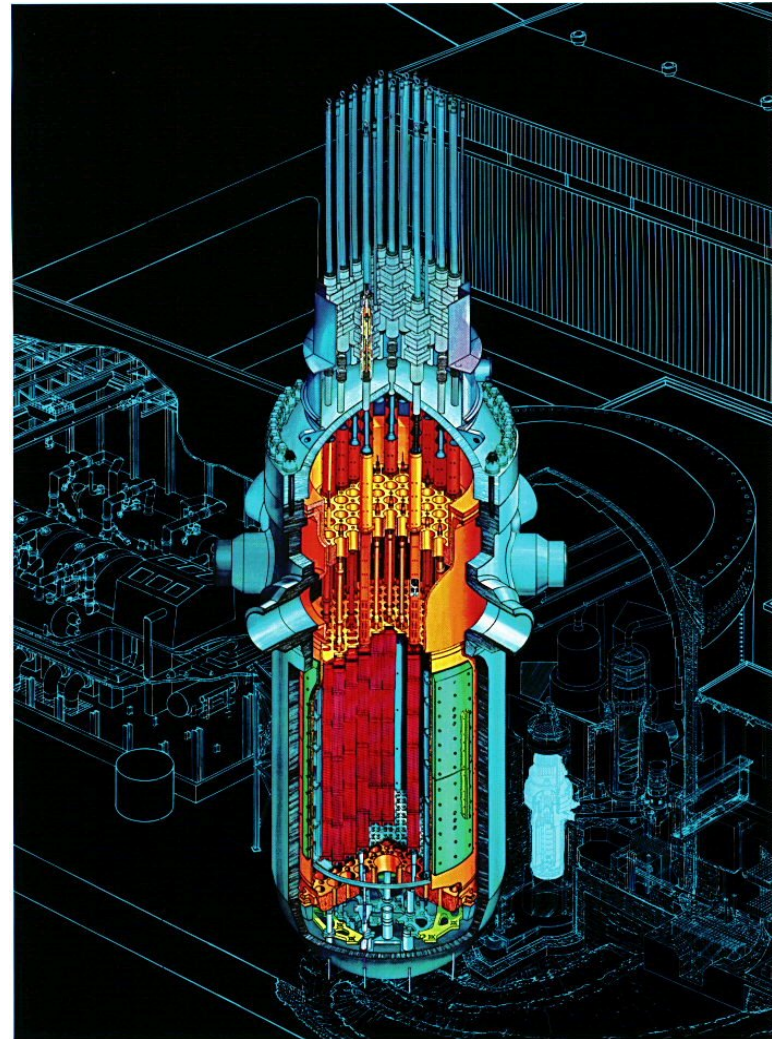
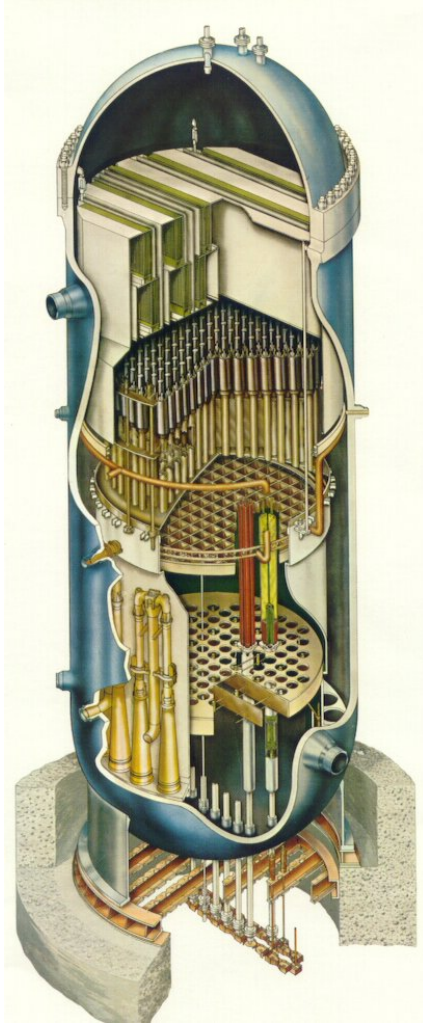
- Overview

- Failure of the Reactor Pressure Vessel (RPV) cannot be considered a credible event
- Highest standards for design, fabrication, operation, inspection
- Service experience has been very good
 - No inservice flaws in the vessel shell

NDE of Pressure Vessels: Practical considerations

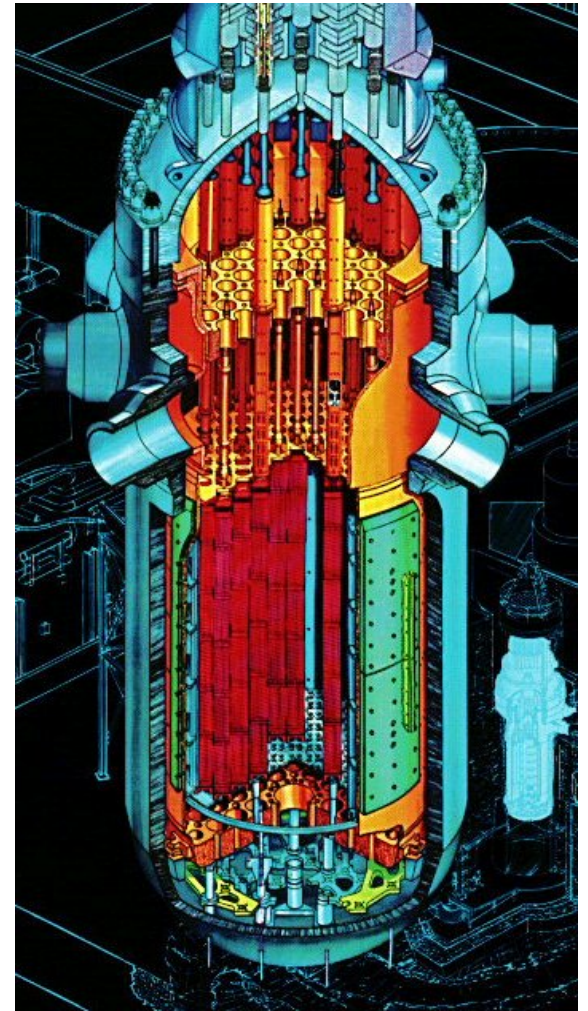
- High safety significance
- Thick sections, sometimes complex geometry
- Difficult access
 - Inspection from inside surface must be performed using remote, automated equipment
 - Inspection from outside has poor access and high radiation levels
 - Mostly performed using automated equipment
 - Specific areas can be picked up using manual UT
- In-vessel time is precious; critical path is nominally worth \$1M/day

BWR and PWR Vessel Cutaways



PWR Pressure Vessel

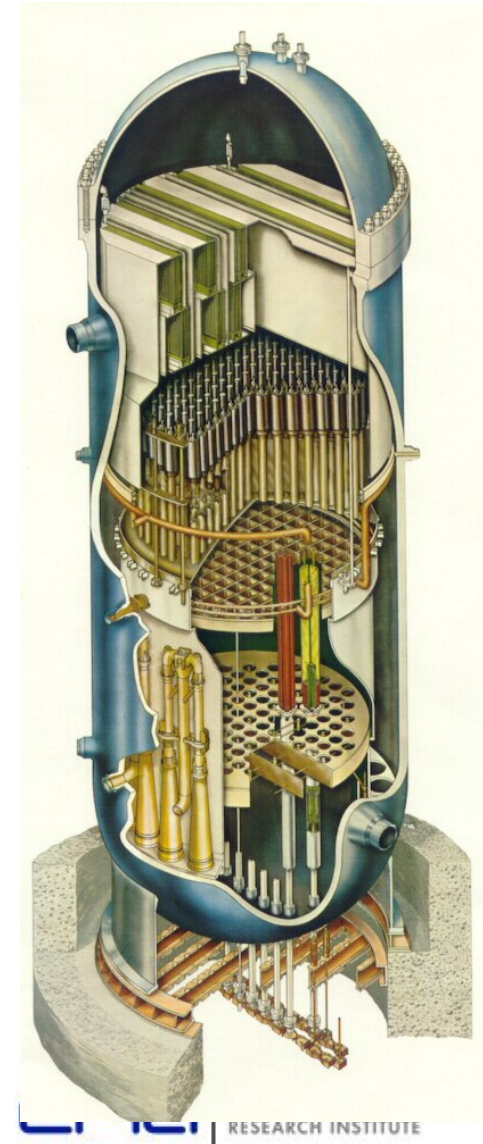
- PWR vessels are examined from the inside surface after removal of internals
- Robotic inspection only, no personnel access
 - Inspect the inlet and outlet nozzle-to-safe end welds at this time
 - Scanned on the inside surface
 - Special end-effectors mounted on the RPV inspection tool



BWR Pressure Vessel

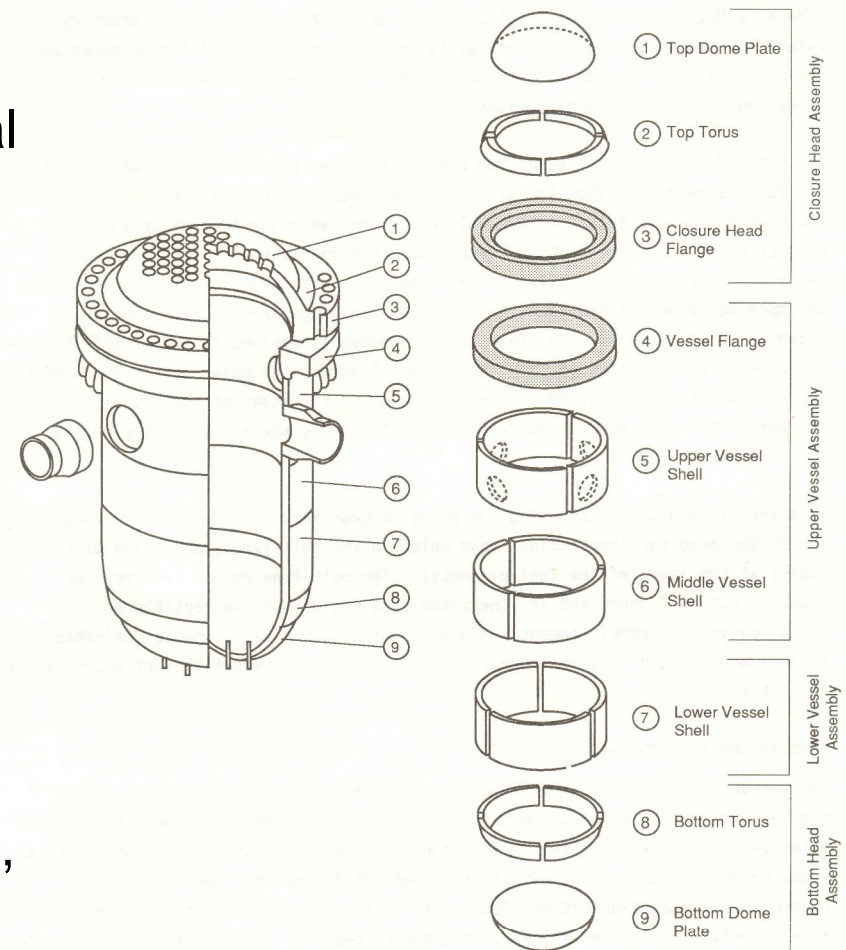
BWR vessels have complex internal structures, some of which cannot be removed

- Examination from the vessel outside surface is preferred (easier and cheaper)
 - Coverage limitations because of obstructions
- Examination from the inside surface usually is also necessary in order to comply with requirements for minimum coverage (90% of weld length)



Vessel Components

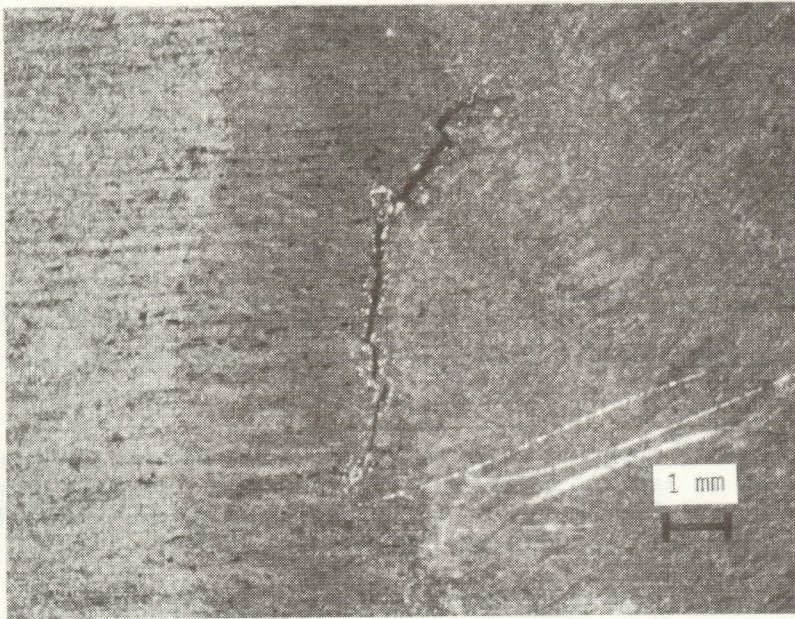
- Shell
 - Assembled from ring forgings or formed plates; vertical and horizontal welds
 - Nozzle-to-shell welds
 - Flange for bolting on the top head
- Top head
 - Assembly welds
 - Penetrations
 - Flange for bolting it onto the vessel
- Bottom head
 - Assembly welds
 - Penetrations
- Cladding
 - Inside surfaces of vessel and heads are covered with stainless steel clad, applied as weld metal



Inservice Inspection

- Base metal of the shell forgings or plates is not normally inspected
- Shell-to-shell welds are examined with ultrasonics
 - Critical area of concern is the inner part of the wall thickness, near the cladding
 - Higher stress and stress intensity
 - Higher embrittlement
 - Possibility of thermal shock

Crack in Backgouged Area of Vessel Shell Weld

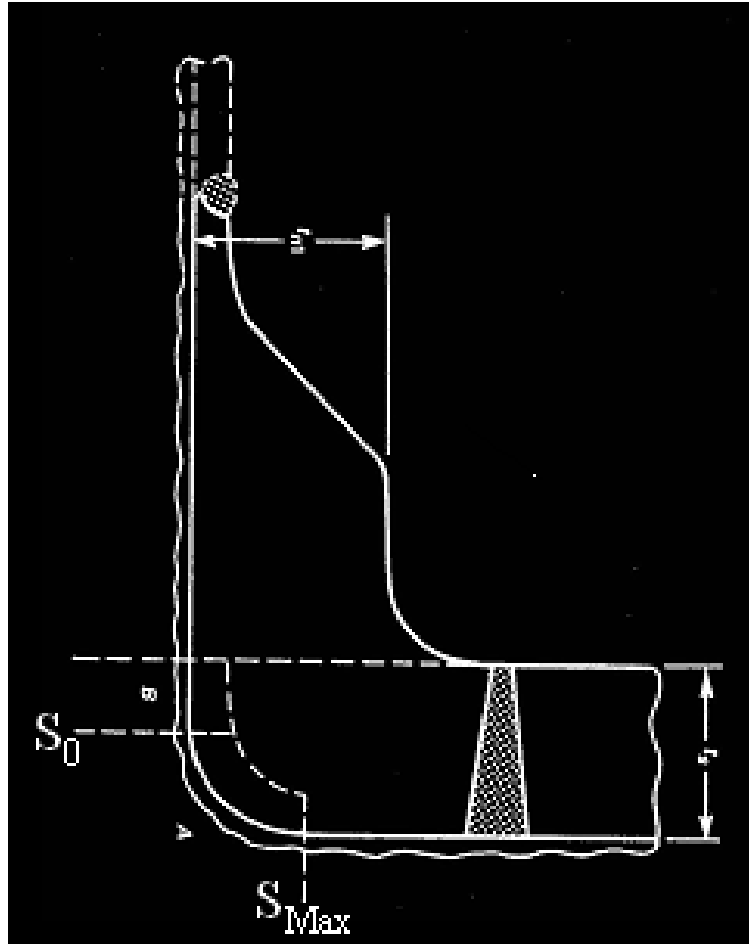


Crack in root area
of double-V weld
in 10" thick vessel
shell

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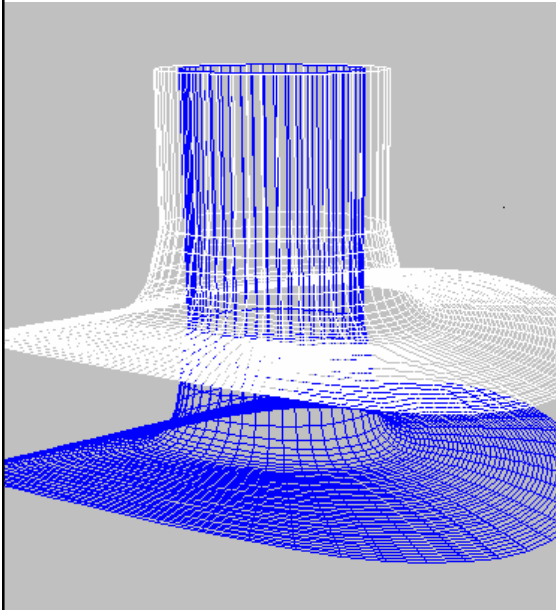
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Nozzle-to-Shell Welds and Nozzle Inner Radius

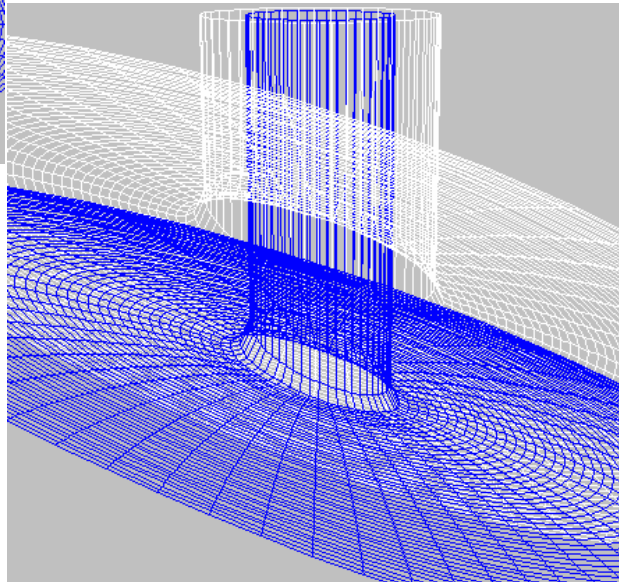


Examination of the nozzle is challenging due to the complex three-dimensional configuration

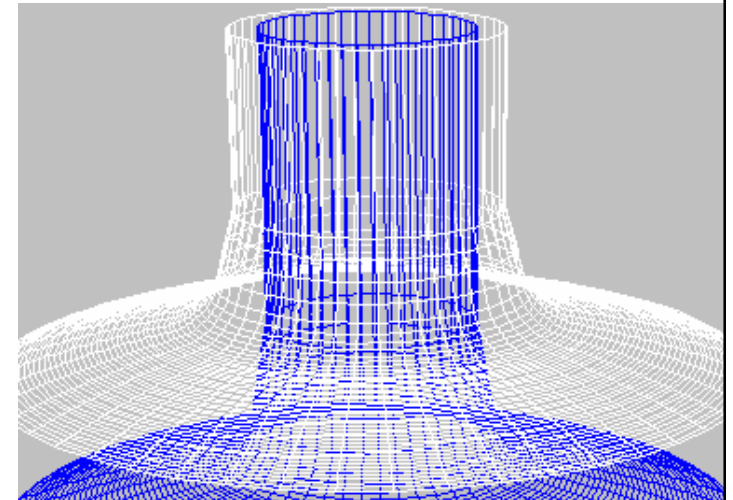
Vessel Nozzle Geometries



Cylinder-to-cylinder



Off-axis



Cylinder-to-sphere

Determining Flaw Location in Nozzle Inner Radius by Geometric Modeling

EPRI 3D Nozzle Modeling Toolkit V1.0R1

File Modeling Direction View Window Help

Forward Modeling

Flaw Type
☒ NIR ☐ NSW

Probe Name: Default Probe

Probe Angle (deg): 31.225059

Probe Skew (deg): 132.83703

Probe R (in): 27 TanPt0 R, Z (26.50, 160.00)

Probe Theta (deg): 65 TanPt1 R, Z (26.50, 160.00)

Probe Z (in): 132.24428 TanPt2 R, Z (26.50, 134.59)

User Metal Path (in): 11 TanPt3 R, Z (31.13, 128.95)

TanPt4 R, Z (50.00, 123.98)

Find Inside Surface (User Metal Path > 0)
 Angle Between Rays: 1.89
☒ Metal Path Diff: 0.000, 0.00%
 Probe Angle Diff: -1.23
 Probe Skew Diff: -2.84

Transducer Parameters

Wedge Base Length (in): 2

Wedge Front Height (in): 1

Wedge Back Height (in): 0.25

Wedge Top Length (in): 0.75

Wedge Width (in): 2

NIR Flaw Forward Results

Flaw R (in), Theta (deg), Z (in), S (in), Loc 20.68, 52.19, 124.95, 7.71, Inner-Blend

Probe R (in), Theta (deg), Z (in), Loc 27.00, 65.00, 132.24, Outer-Blend

Probe Angle (deg), Skew (deg), Metal Path (in) 31.23, 132.84, 11.00

Beam/Skew Angle at Flaw (deg), Misorientation Angle (deg) 38.19/128.48, 38.48

Conf Probe R (in), Theta (deg), Z (in), Loc 27.13, 41.98, 133.38, Outer-Blend

Conf Probe Angle (deg), Skew (deg), Metal Path (in) 32.58, -135.79, 11.43

Beam/Conf Skew Angle at Flaw (deg), Conf Misorientation Angle (deg) 38.19/-128.48, 38.48

Scale and Move

Scale X,Y,Z
☒ Up ☐ Down 3

Trans Nozzle X: 0

Trans Nozzle Y: 0

Trans Nozzle Z: -70

Rot Abt Nozzle X: 0

Rot Abt Nozzle Y: 0

Rot Abt Nozzle Z: 0

EPRI 3D Nozzle Modeling Toolkit V1.0R1-View

File Options

Flaw R (in), Theta (deg), Z (in), S (in), Loc 20.68, 52.19, 124.95, 7.71, Inner-Blend

Probe R (in), Theta (deg), Z (in), Loc 27.00, 65.00, 132.24, Outer-Blend

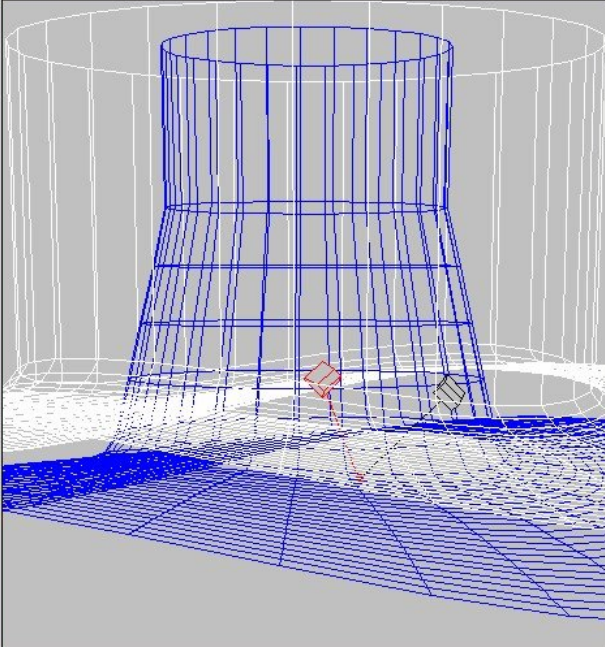
Probe Angle (deg), Skew (deg), Metal Path (in) 31.23, 132.84, 11.00

Beam/Skew Angle at Flaw (deg), Misorientation Angle (deg) 38.19/128.48, 38.48

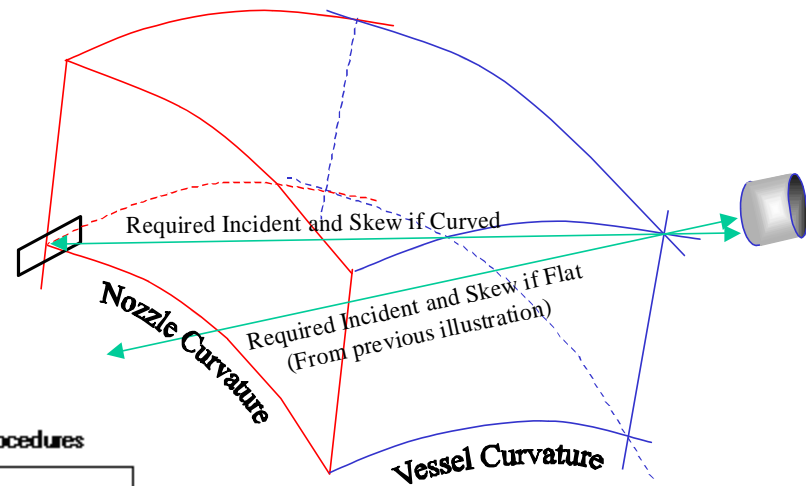
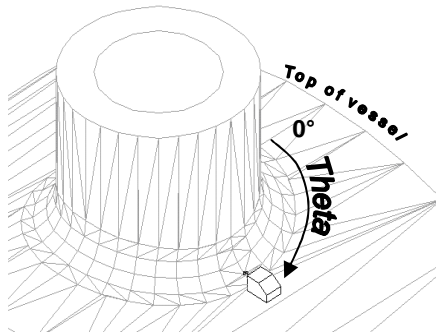
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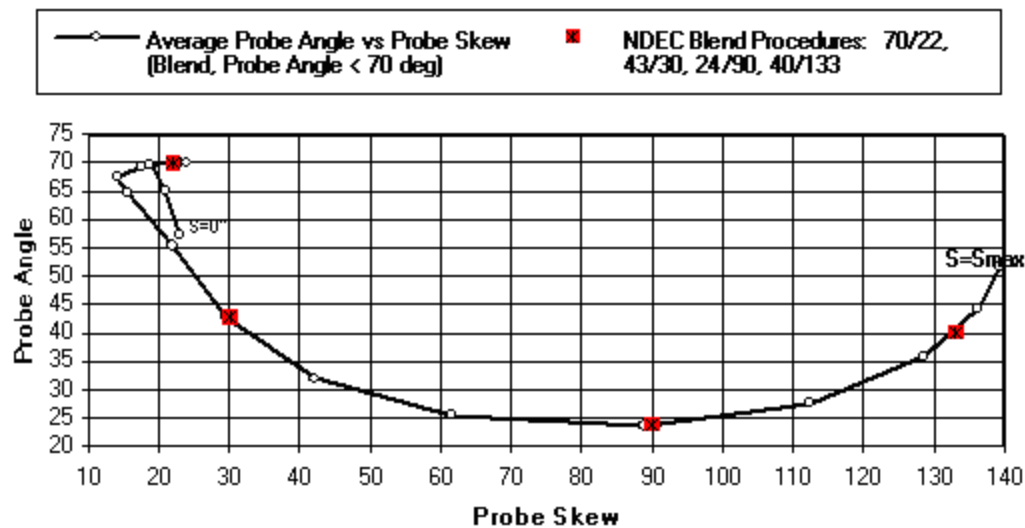
Beam/Conf Skew Angle at Flaw (deg), Conf Misorientation Angle (deg) 38.19/-128.48, 38.48



Nozzle-to Shell Welds



Feedwater Nozzle: Probe Angle vs Probe Skew and NDEC Procedures

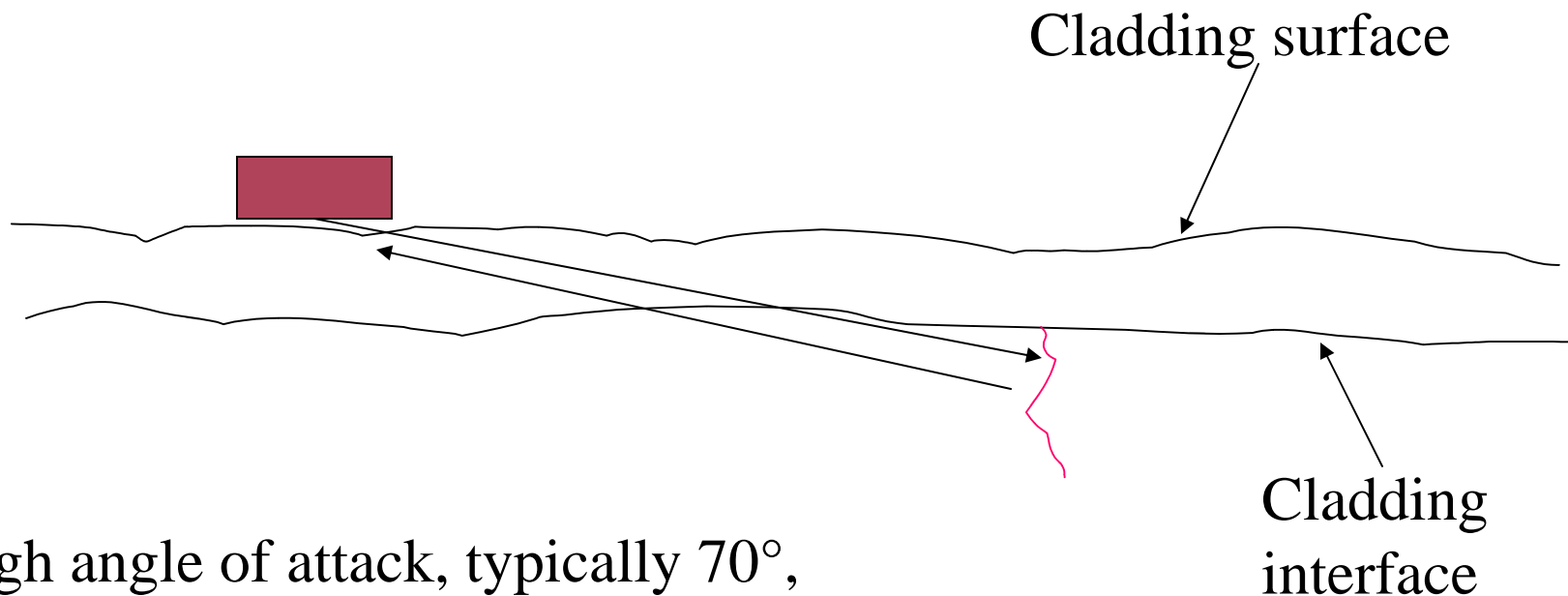


Computer modeling is necessary to optimize the procedures, locate indications, and control the mis-orientation angles within qualified ranges

Outline

- What's NDE?
- NDE for stainless steel and nickel-alloy components
 - Piping
 - Dissimilar metal welds
 - Cast stainless steel
 - Reactor pressure vessel head penetrations
- NDE for reactor pressure vessels
 - Vessel overview
 - Nozzles
 - Underclad cracking
 - Qualification
 - Example of plant-specific vessel NDE issue
- Summary

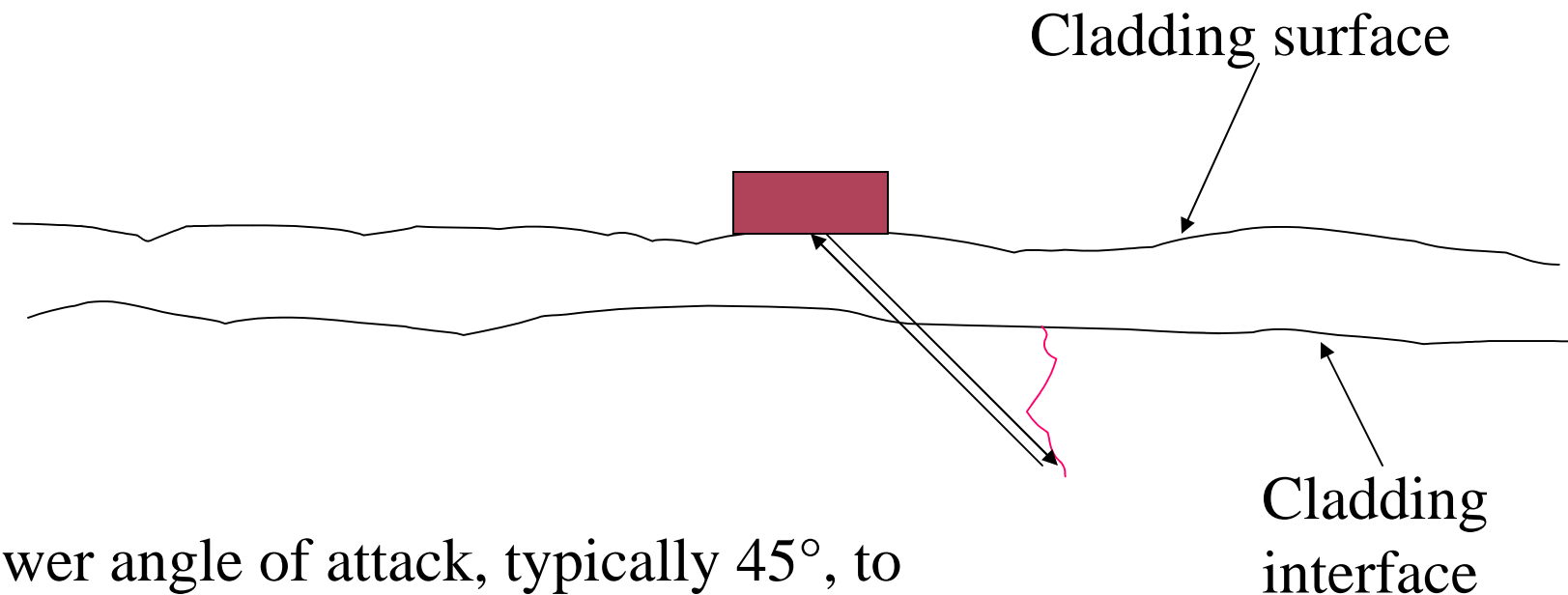
Examination Methods for Detection of Underclad Cracking



High angle of attack, typically 70° ,
to maximize reflectivity

Good for detection and length sizing,
but depth sizing isn't accurate

Examination Methods for Depth Sizing of Underclad Cracking



Lower angle of attack, typically 45° , to maximize accuracy of locating tip

Good for depth sizing, but the response is low-amplitude and less reliable for initial detection

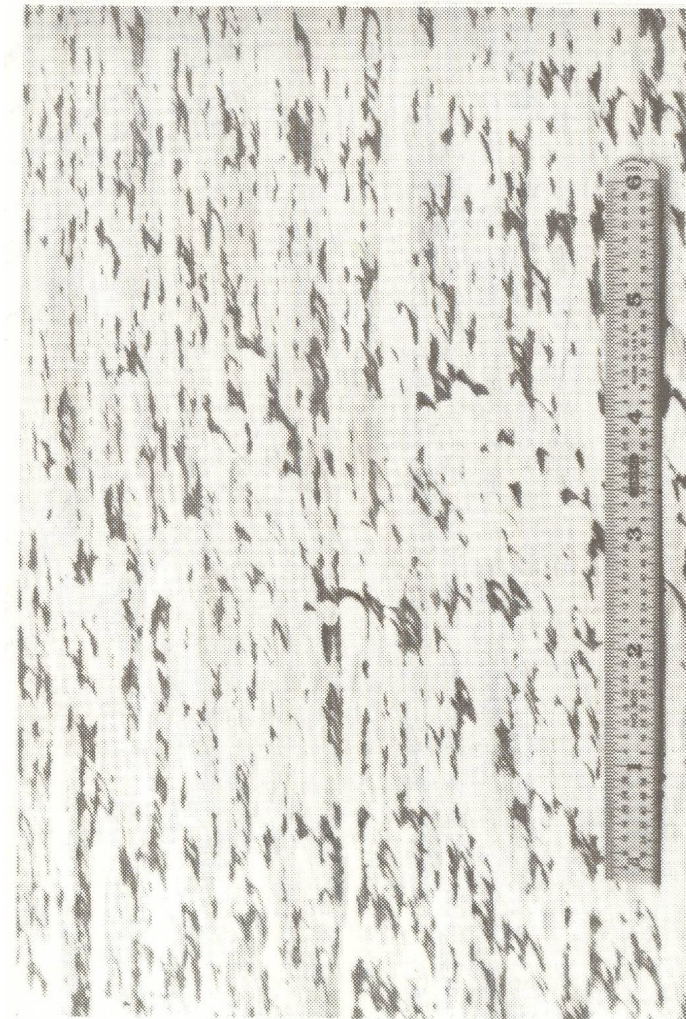
Cladding Effects

- Vessel cladding is weld deposited
 - It's stainless steel weld metal, so it's anisotropic
 - Highly attenuative
 - Noisy
 - Can change the direction of the sound beam in erratic ways
 - Surface condition also affects UT
- The good news – we don't have to detect flaws in the cladding itself, because no structural credit is taken for it

Vessel Cladding-Surfaces

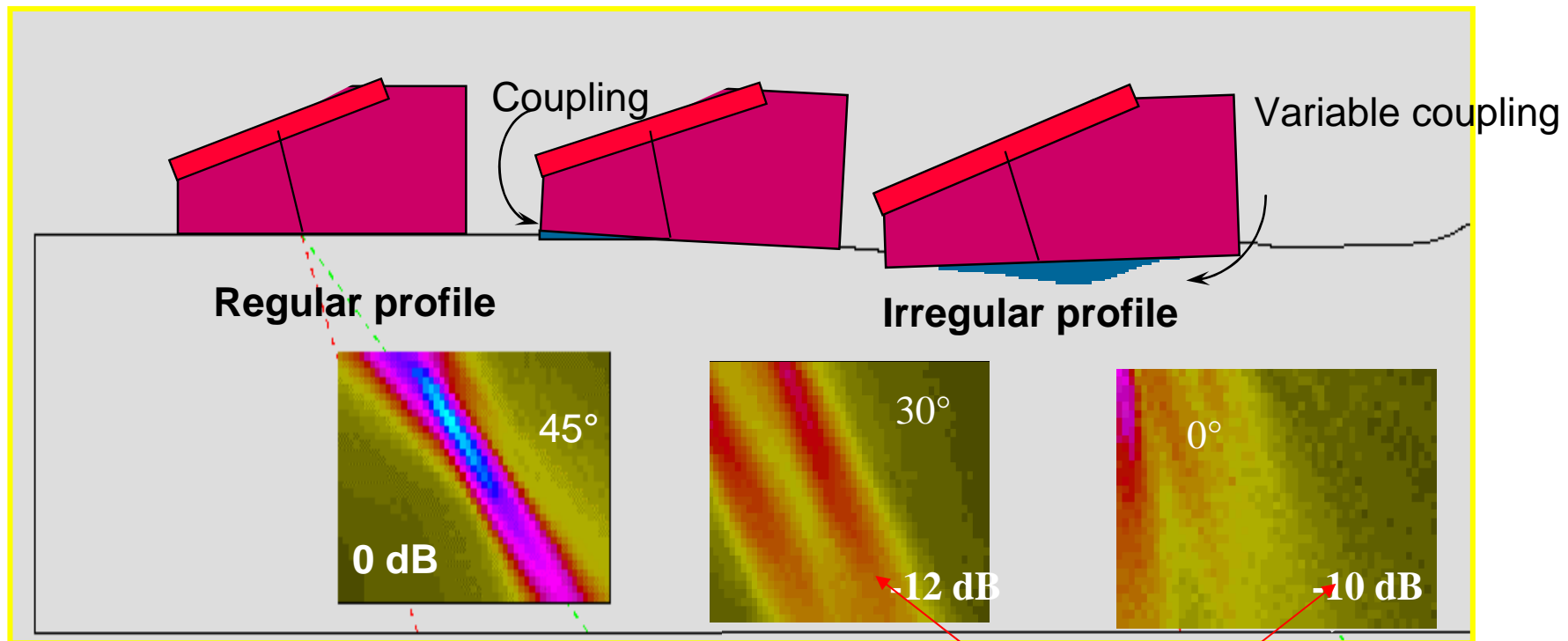


Automated welding



Manual welding

Cladding Roughness Lens Effect – Where's the Beam Going?



**Nominal beam
characteristics**

**Degraded and distorted
beam**

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Qualification

- Proof that NDE procedures, personnel, and equipment can detect and properly characterize flaws
 - Use of realistic flaws in realistic mockups
- Total cost of program to date is in tens of millions
 - Mockup cost
 - Administrative cost
- Qualification is impactful
 - RPV procedure qualification may take months, and cost the vendor ~\$0.5M

Qualification for RPV in the US

- Procedure qualification (NDE services vendor)
 - Several mockups must be examined
 - Total of 30-60 defects; all defects must be detected
 - Defect size measurement accuracy requirements
 - Length: RMS value of errors < 0.75 inch (19 mm)
 - Depth: RMS value of errors < 0.125 inch (3 mm)
- Personnel qualification (Vendor or utility personnel)
 - 10 – 20 defects
 - A small number of defects may be missed
 - A small number of false calls are allowed
 - Sizing accuracy criteria are the same as above

RPV Mockups



RPV Mockups



RPV Mockups



Outline

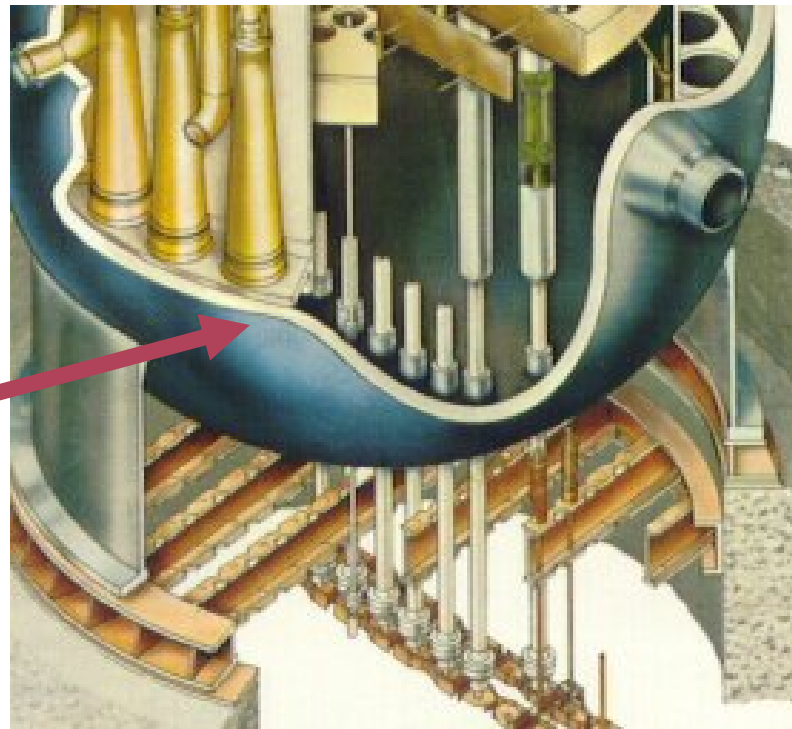
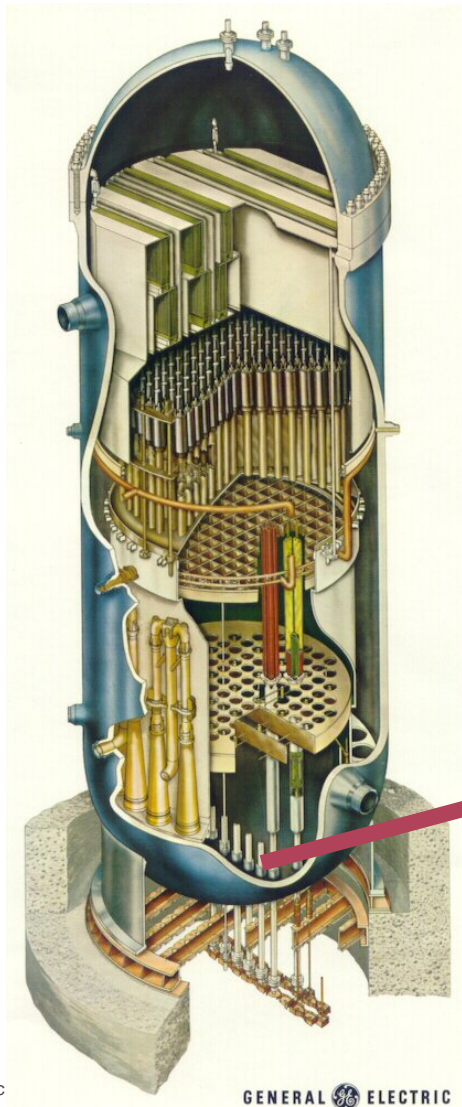
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Practical Example of an RPV Issue: Leak from BWR RPV Bottom Head

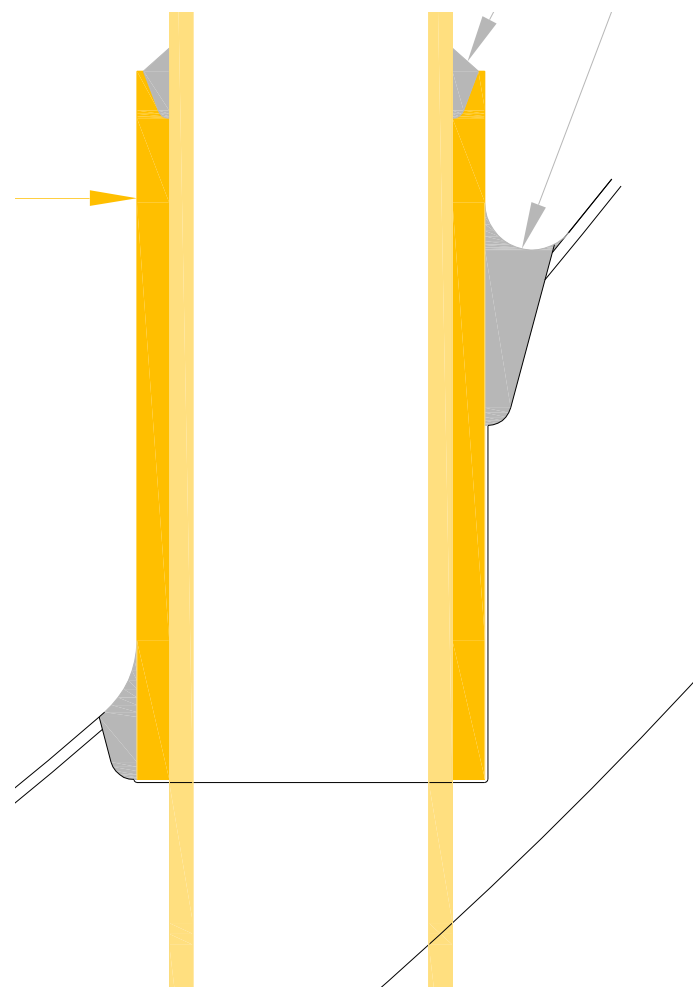
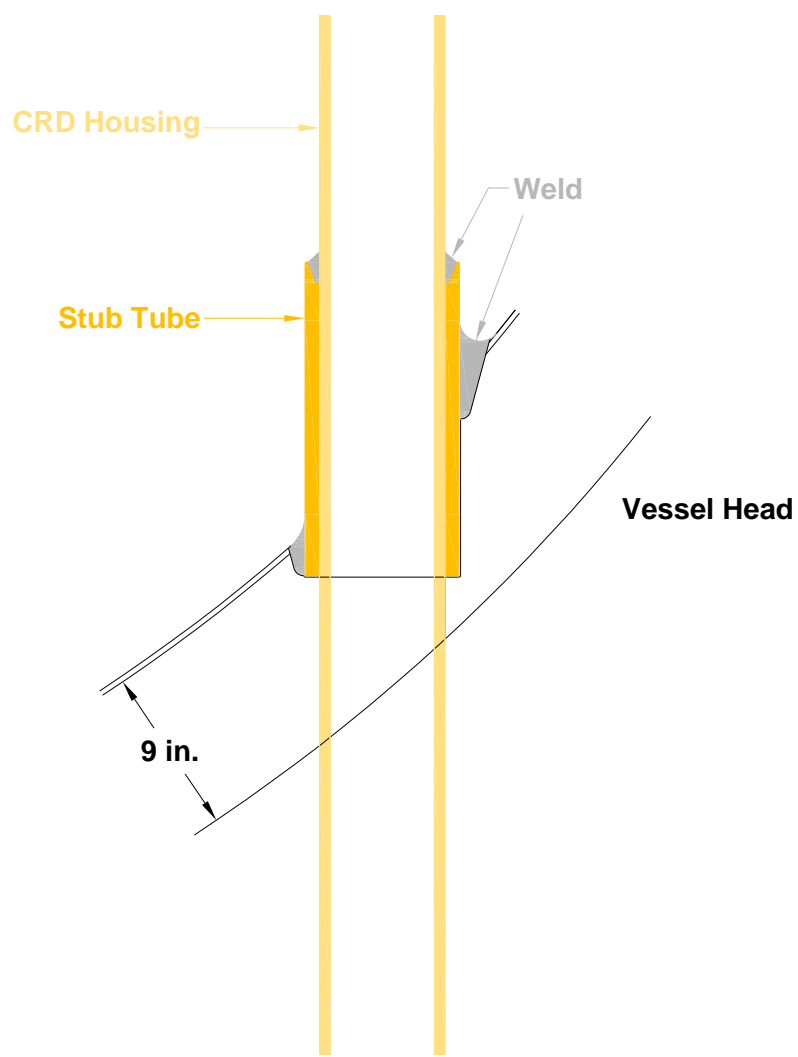
- Next several slides will illustrate an example of a vessel-related field inspection issue
 - Plant concern
 - EPRI response
 - Field application

Practical Example: Bottom Head Leak **Background**

- **Bottom head of BWR RPV has many tubes coming through it (control rod drive mechanism housings, mostly)**
- **Nine Mile Point Unit 1 saw evidence of leakage under the head, at one of the CRDM penetrations**



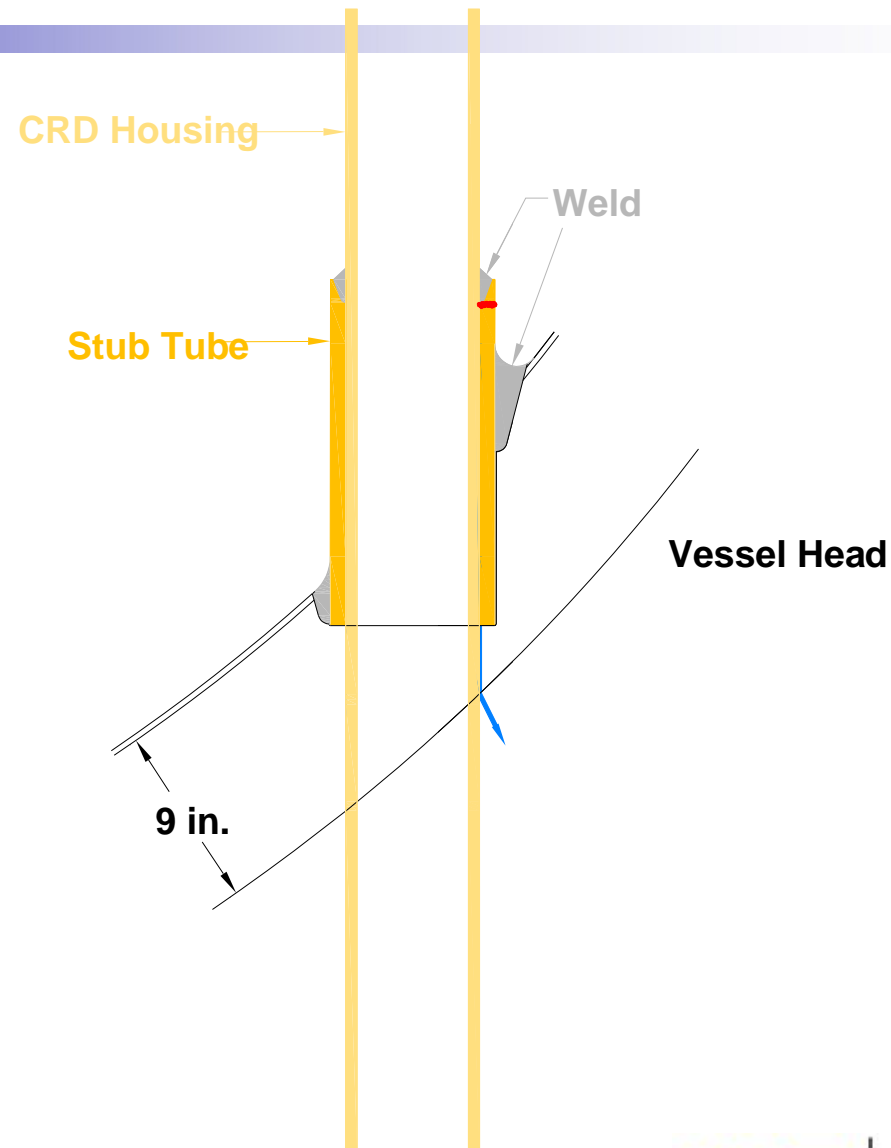
Practical Example: Bottom Head Leak Stub Tube Design



Practical Example: Bottom Head Leak

History of leakage through cracks in the tube

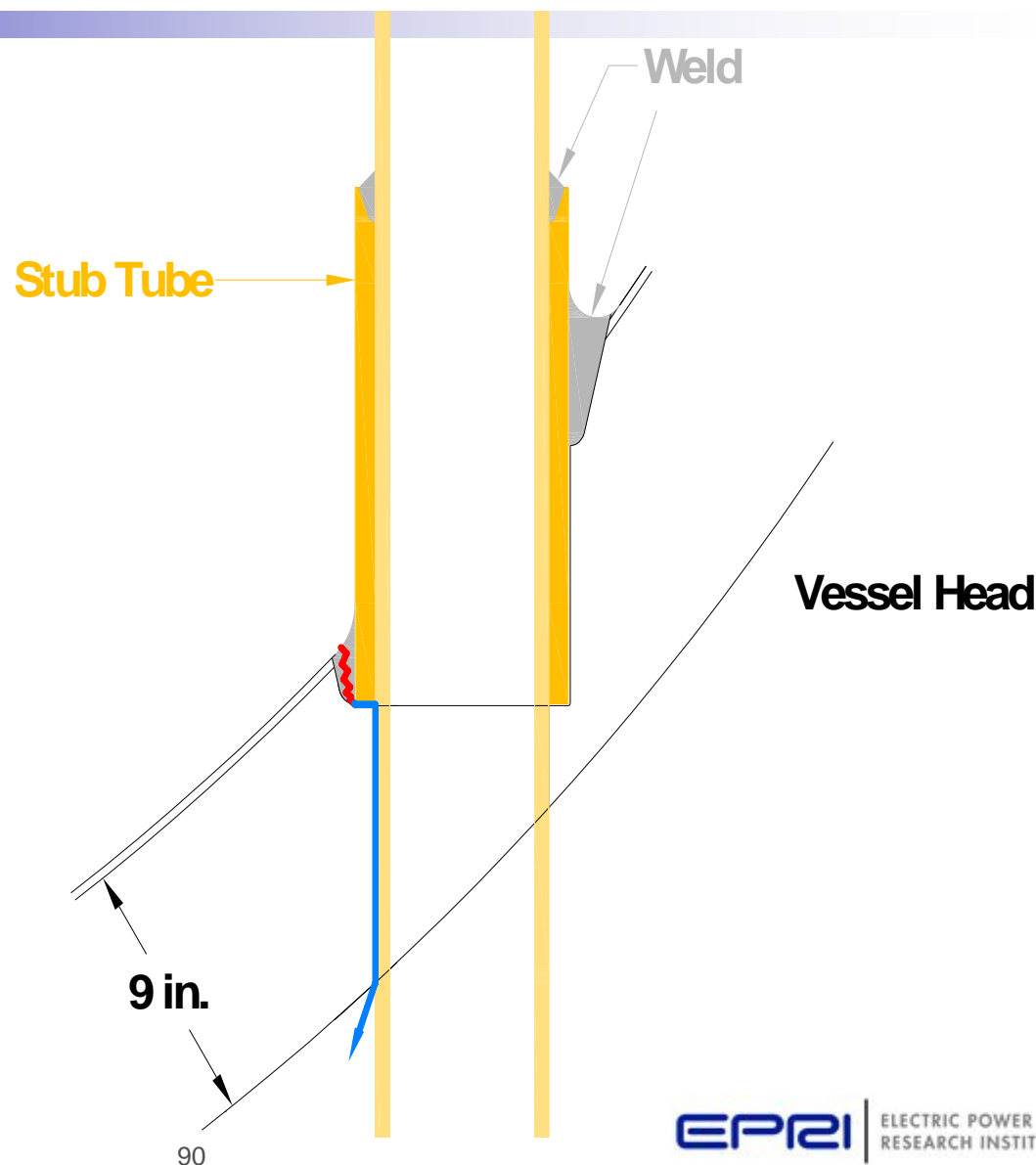
- This design has experienced several leaks due to cracking of the stub tube
 - Not a vessel integrity issue



Practical Example: Bottom Head Leak

Recent experience at a Japanese plant

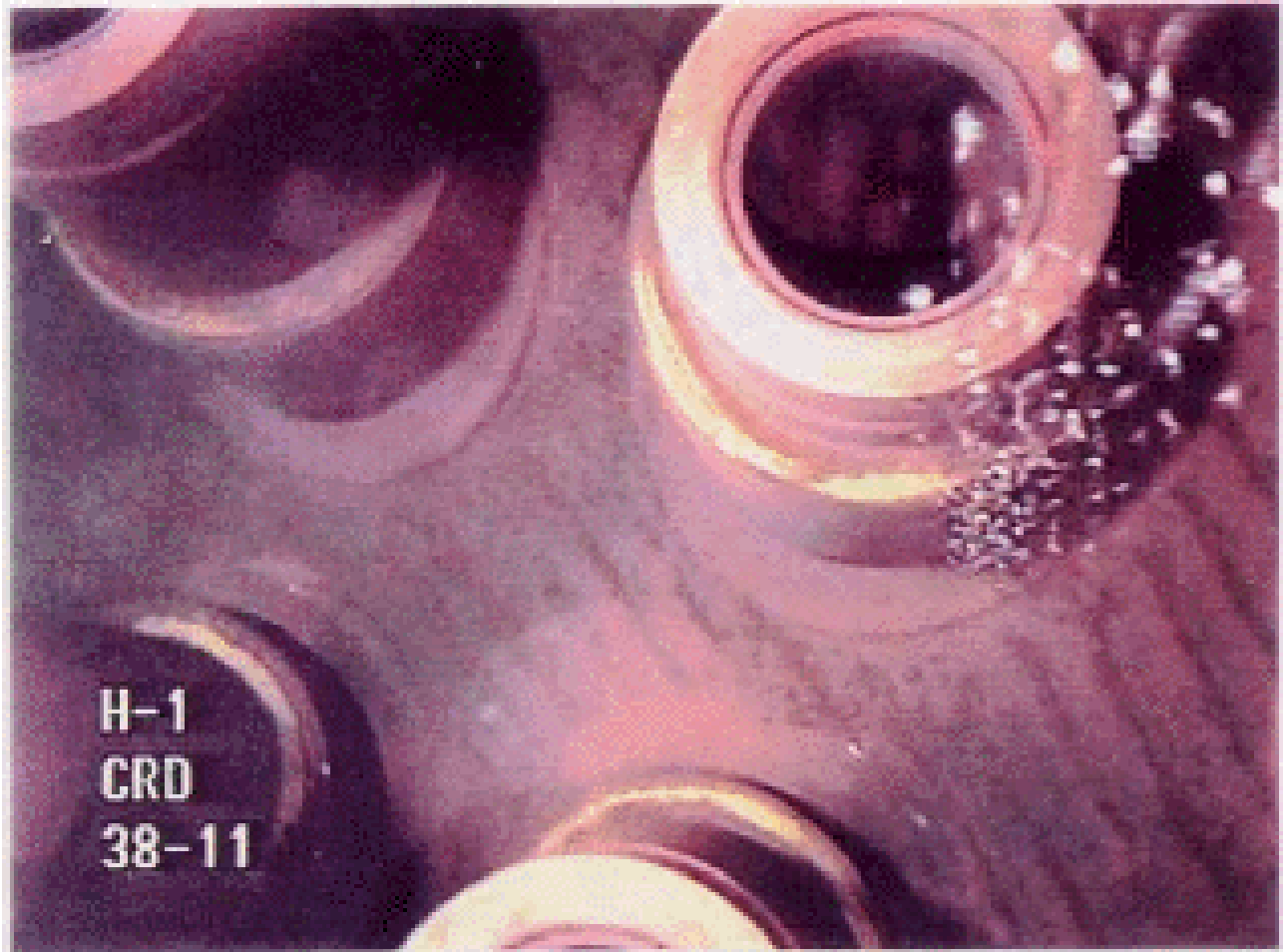
- Recently a plant in Japan experienced a similar leak, but from a much more serious location: the stub tube-to-vessel weld
- If the weld crack grows into the vessel steel, the vessel faces a serious structural integrity issue



Practical Example: Bottom Head Leak

Recent Japanese leak from a weld crack

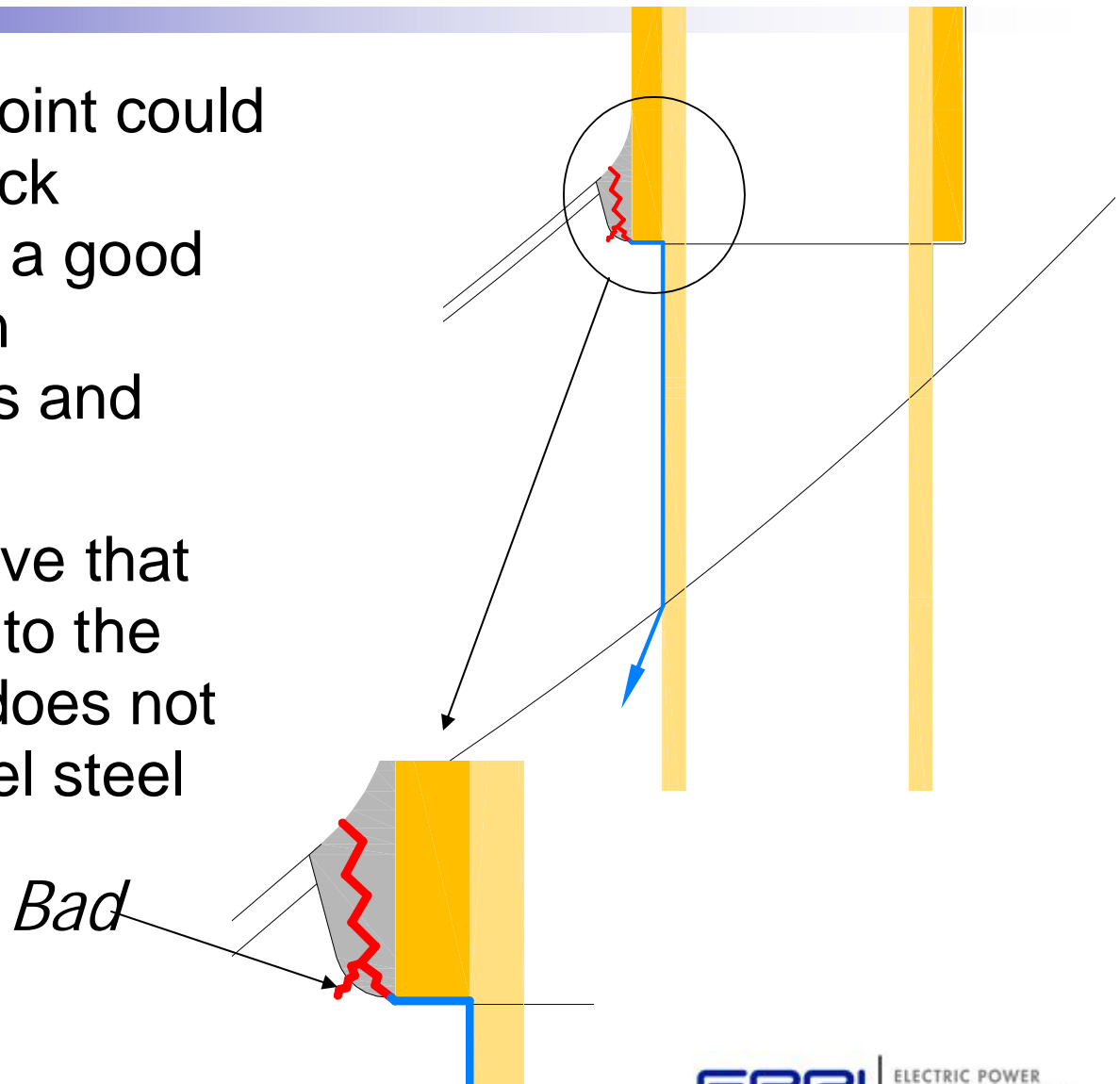
- Crack was repaired at a cost of \$100M
- Crack did not grow into the vessel
- Nine Mile Point planned a visual examination to see whether its leak was coming from a tube crack or a weld crack



Practical Example: Bottom Head Leak

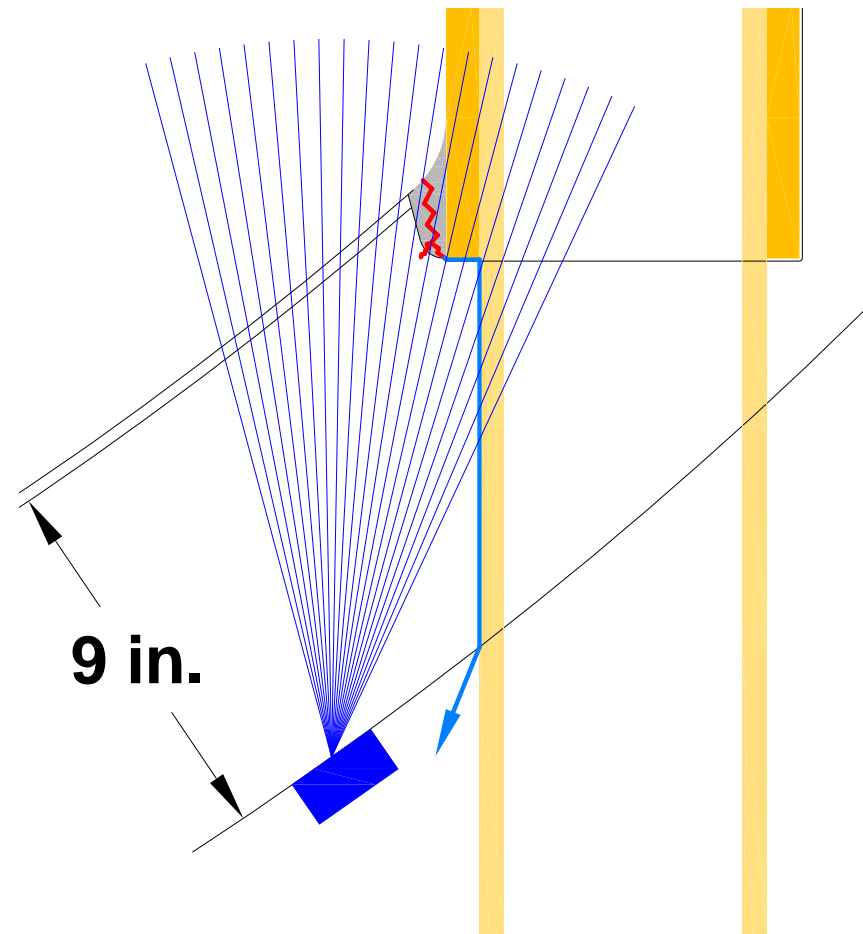
Vessel integrity issue

- Maybe Nine Mile Point could live with a weld crack without repair, with a good argument based on materials properties and stress fields, but ...
- The utility must prove that the crack is limited to the weld volume, and does not penetrate the vessel steel



Practical Example: Bottom Head Leak **Phased Array UT Solution**

- How to determine whether the crack is limited to the weld volume?
- Solution: use phased array ultrasound technology
 - Maximum coverage can be achieved from limited accessible scanning area

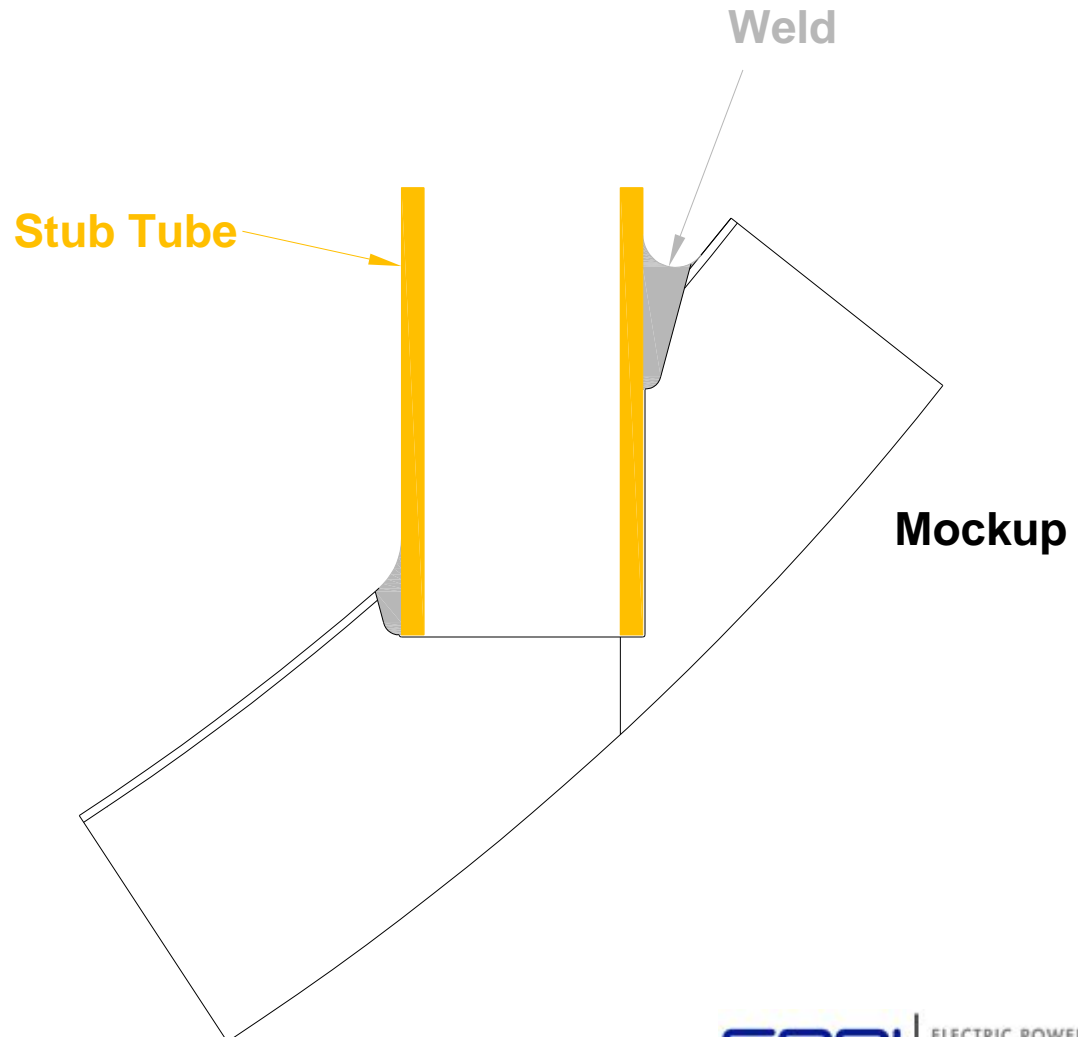


Practical Example: Bottom Head Leak

Mockup Development

Mockups

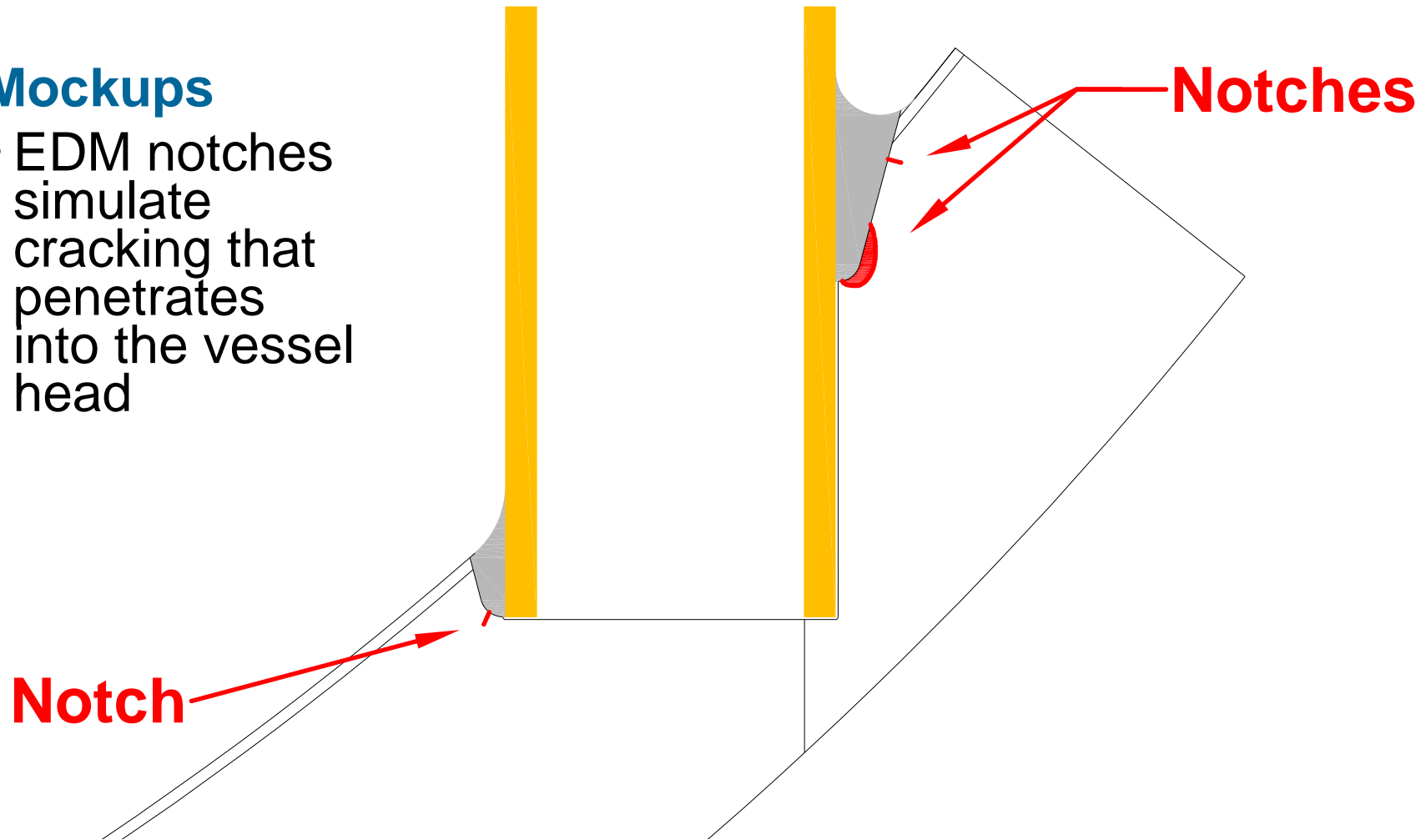
- Used existing material to build two realistic mockups



Practical Example: Bottom Head Leak **Mockup Development**

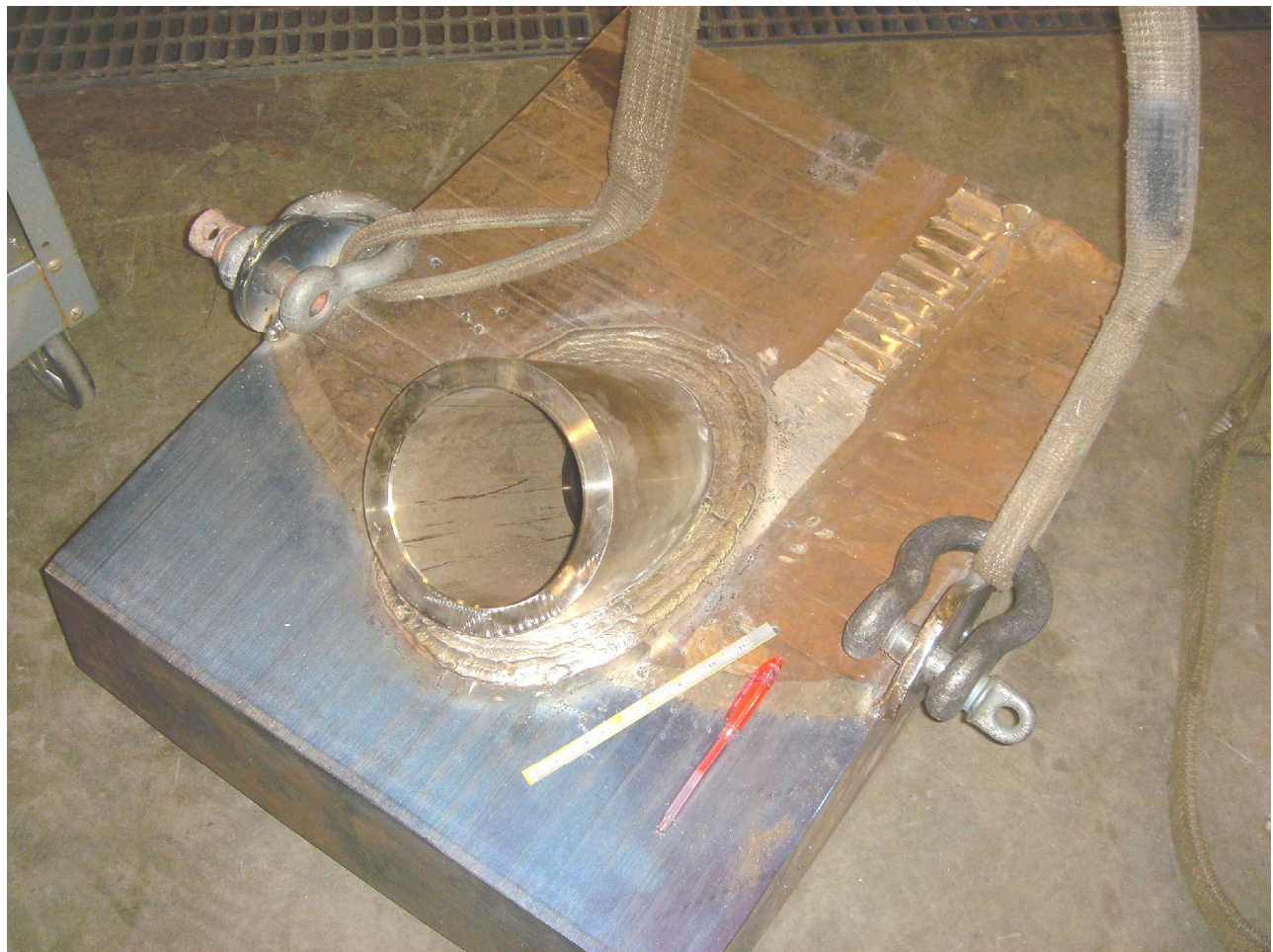
Mockups

- EDM notches simulate cracking that penetrates into the vessel head



Practical Example: Bottom Head Leak
Mockup Development

Mockups



Practical Example: Bottom Head Leak **Mockup Development**

Mockup notches

- Irregular tip shape



Practical Example: Bottom Head Leak

Ultrasonic Response from a Notch

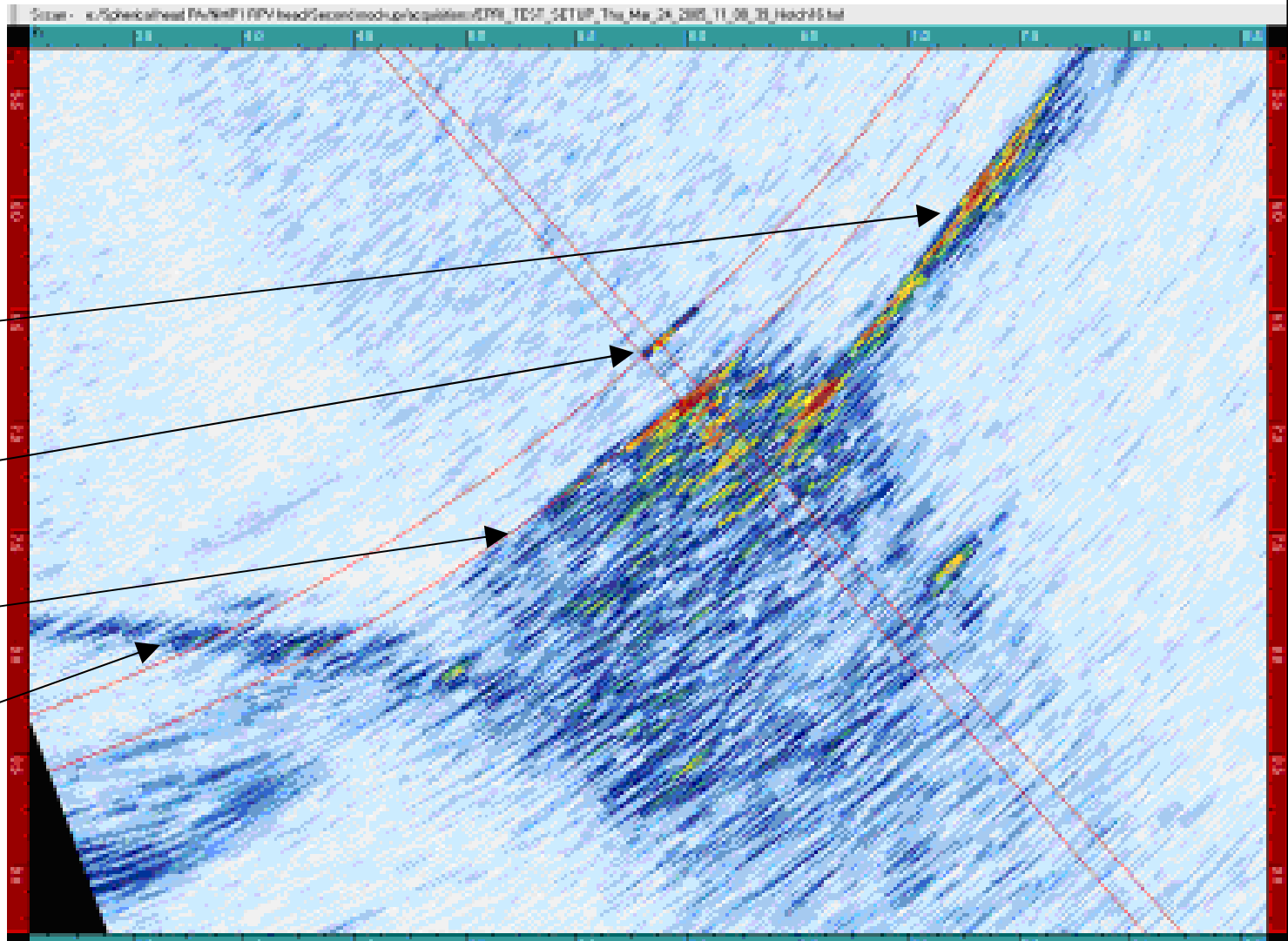
Sample image

Vessel penetration response

Notch tip response

Weld noise

Inside surface clad response



Practical Example: Bottom Head Leak Inspection Capability

- All notches were detectable
- Sizing accuracy good

| Notch | Location on weld prep | True penetration | Measured penetration | Error |
|------------|-------------------------|-----------------------------|----------------------|--------------|
| 11 | Radius and top of taper | 0.30 | No measurement | |
| 12 | Radius and top of taper | 0.30 | 0.32 | +0.02 |
| 13 | Radius | 0.26 | 0.23 | -0.03 |
| 14 | Radius and top of taper | 0.20 | 0.17 | -0.03 |
| 15A (up) | Top of taper | 0.25 | 0.24 | -0.01 |
| 15B (up) | Bottom of taper | 0.25 | 0.17 | -0.08 |
| 15A (down) | Top of taper | 0.25 | 0.20 | -0.05 |
| 15B (down) | Bottom of taper | 0.25 | 0.21 | -0.04 |
| 16 (up) | Top of taper | 0.30 | 0.29 | -0.01 |
| 16 (down) | Top of taper | 0.30 | 0.27 | -0.03 |
| 17 | Top of taper | 0.26 | 0.22 | -0.04 |
| 18 | Top of taper | 0.30 | 0.30 | 0.00 |
| | | | | |
| | | Average error (inch) | | -0.03 |

Practical Example: Bottom Head Leak
Field Application

Inspection was not performed

- No visual evidence of further leakage
- No cracking was observed in stub tube-to-vessel weld
- Utility did not perform the UT examination
 - Radiation exposure
 - Logistical difficulty

Summary – Pressure Vessel

- Reactor pressure vessels are inspected with highest levels of quality
- Although ferritic materials are less challenging than austenitic materials to inspect, there are many geometric obstacles to overcome
- Qualification has improved the quality of inspections, but at a significant cost

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Summary - overall

- NDE is a key part of maintaining integrity of the pressure boundary
- Combinations of NDE methods are used to achieve full coverage of the areas of interest
- Qualification by practical test is required
- NDE can have a significant impact on outage scheduling
 - Planning is key